

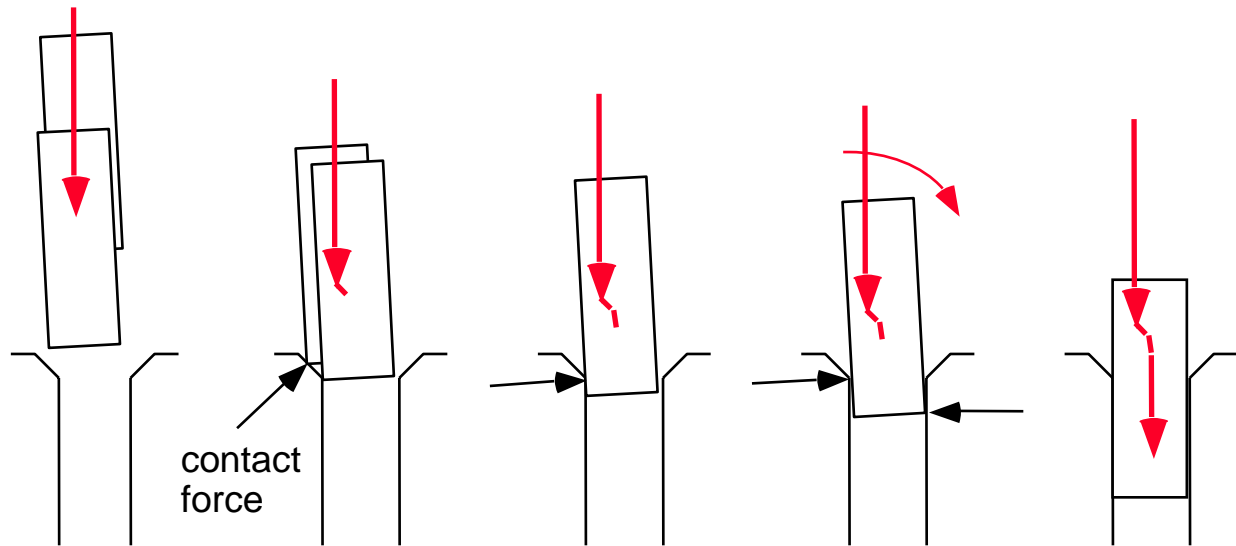
Rigid Part Mating

- Goals of this class
 - understand the phases of a typical part mate
 - determine the basic scaling laws
 - understand basic physics of part mating for simple geometries
 - relate forces and motions arising from geometric errors
 - compare logic branching and direct error-feedback part mating strategies

Basic Bandwidth Issues and Time-Mass-Distance Scaling Laws

- Torque required to move a mass M at the end of an arm of length L in time T is proportional to
 - $M L^2/T^2$
- This implies that really fast motions must be really small or use a small arm with small mass
- I estimated
 - my hand's mass = 250g, effective length = 10cm
 - my arm + hand's mass = 1700g, effective length = 35 cm
 - ratio arm:hand of $ML^2 = T^2 = 85$
- Don't forget: arm mass+payload mass= M

Main Phases of a Part Mating Event



Approach

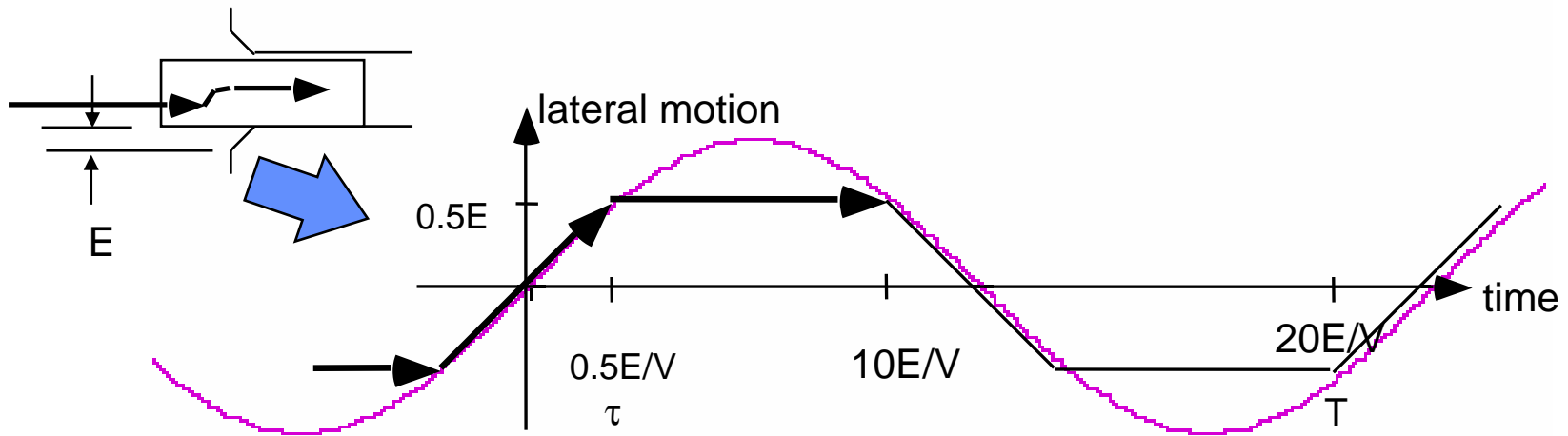
Chamfer
Crossing

One-point
Contact

Two-point
Contact

Line
Contact

Required Bandwidth for Chamfer Crossing



$$\text{Fourier coefficient} = 2 \pi T / (n^2 \pi^2 \tau) \sin (2 n \pi \tau / T)$$

$$T = 20 E / V; \tau = E / 2 V; T / \tau = 40$$

$$\text{Period} = 2\pi = \omega T = \omega 20E/V$$

$$\omega = \pi V / 10 E$$

$$f = V / 20 E$$

$$\text{If } V = 10 \text{ in/s and } E = 0.05", f = 10 \text{ Hz}$$

If 5th harmonic must be adhered to, bandwidth needed = 50Hz

Trapezoidal Wave Harmonics

Image removed for copyright reasons.

Source:

Figure 9-7 in [Whitney 2004] Whitney, D. E. *Mechanical Assemblies: Their Design, Manufacture, and Role in Product Development*. New York, NY: Oxford University Press, 2004. ISBN: 0195157826.

Conclusions

- Gross motions can be (must be) done by large arms that necessarily will move slowly
- No robot arm with practical reach can make fine motion error removal adjustments at 50 Hz
- Fine motions can be fast if they are done by small arms, and must be fast to absorb typical errors at economical speeds
- Big tasks with big parts will take a long time compared to small tasks with small parts
- What we see: small parts cycle times are ~5s while big parts cycle times are ~ 60s.

Essentials of Part Mating Theory for Fine Motions

- Quasi-static assumption
- Geometry of pegs and holes
- Applied forces
- Normal reaction forces and friction reaction forces
- Entry geometry limits
- Wedging conditions
- Jamming conditions
- Alternate strategies for accomplishing fine motion

The Basic Idea

- In gross motions, it pays to pre-plan to prevent errors
- In fine motion, it does not pay to try to prevent errors
- So the principle is to anticipate errors and figure out how to make assembly happen anyway
- This requires us to understand three factors:
 - Geometry
 - Compliance
 - Friction

Geometry of Peg-Hole Mates

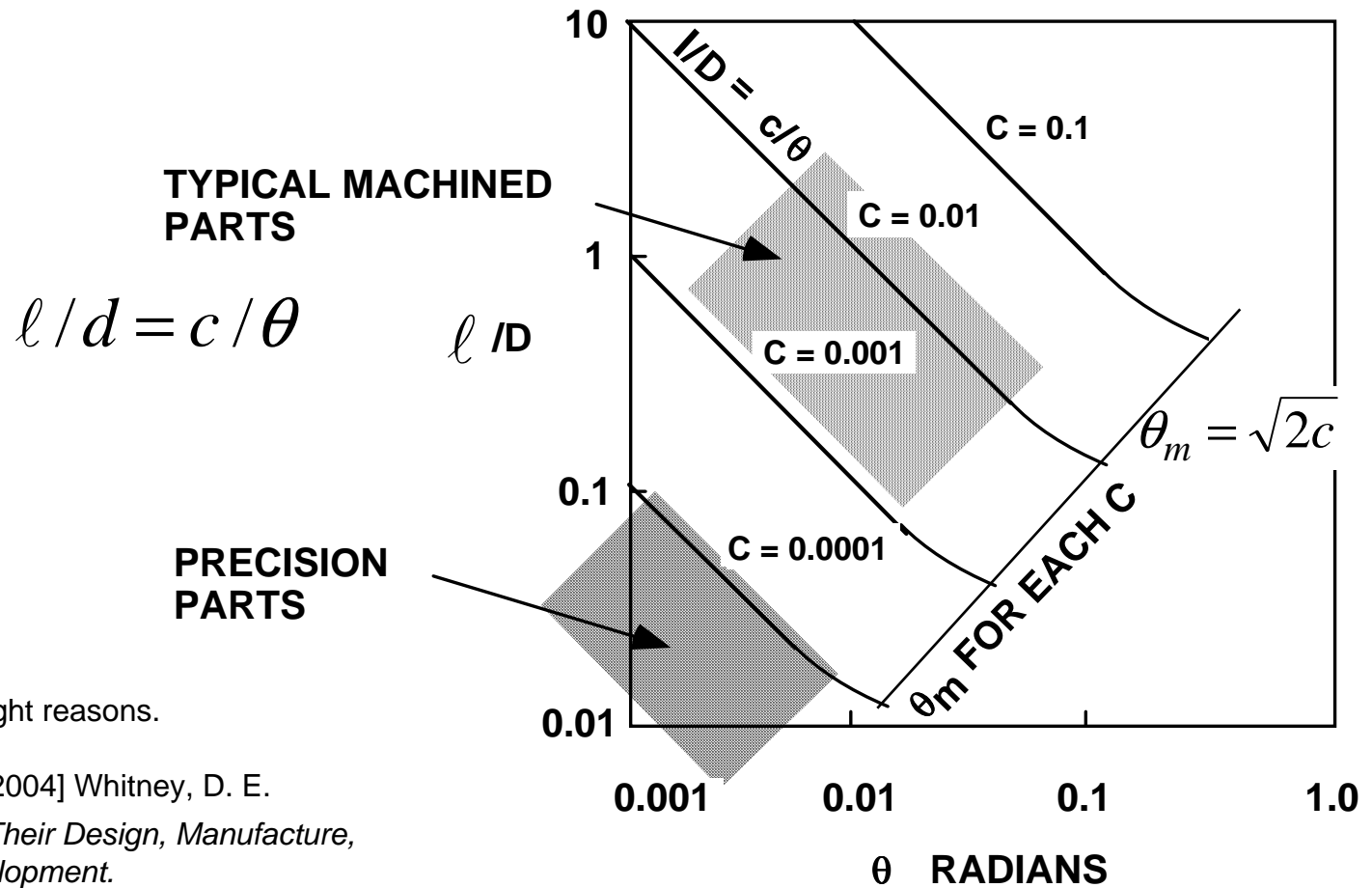


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Source:

Figure 10-15 in [Whitney 2004] Whitney, D. E.

Mechanical Assemblies: Their Design, Manufacture, and Role in Product Development.

New York, NY: Oxford University Press, 2004. ISBN: 0195157826.

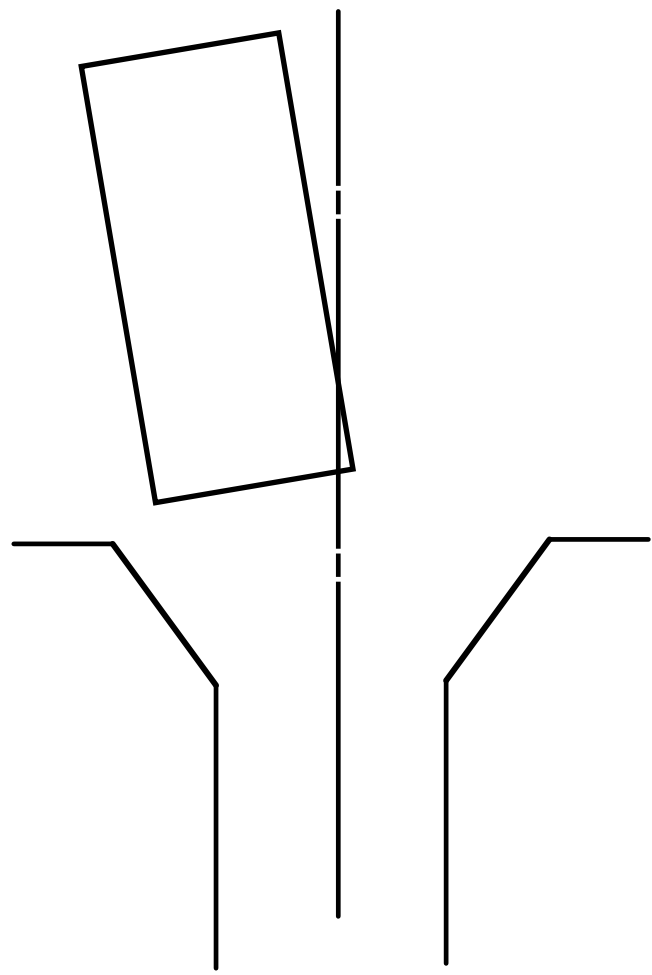
Dimensioning Practice

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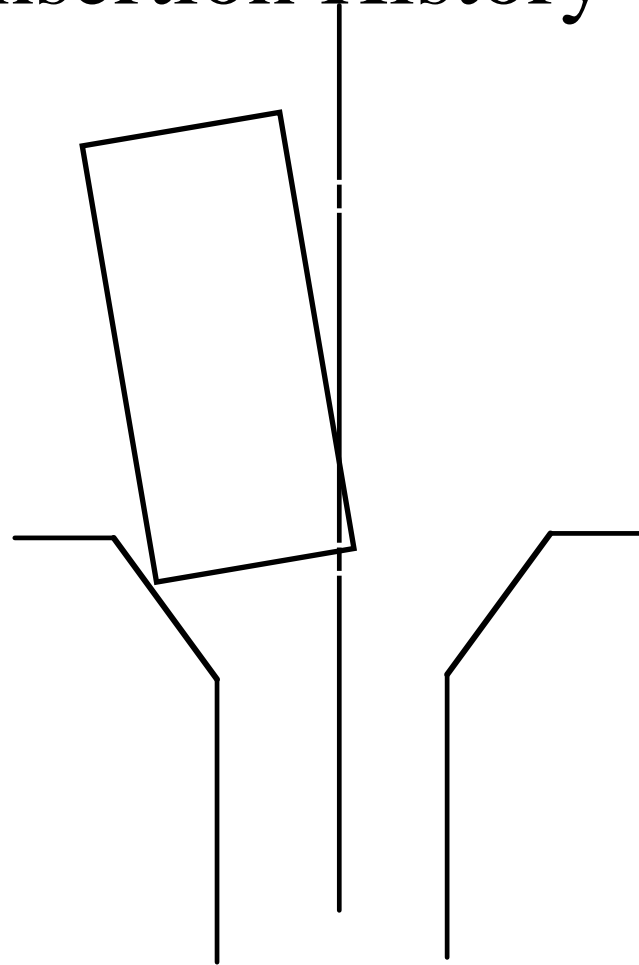
Source:

Figure 10-16 in [Whitney 2004] Whitney, D. E. *Mechanical Assemblies: Their Design, Manufacture, and Role in Product Development*. New York, NY: Oxford University Press, 2004. ISBN: 0195157826.

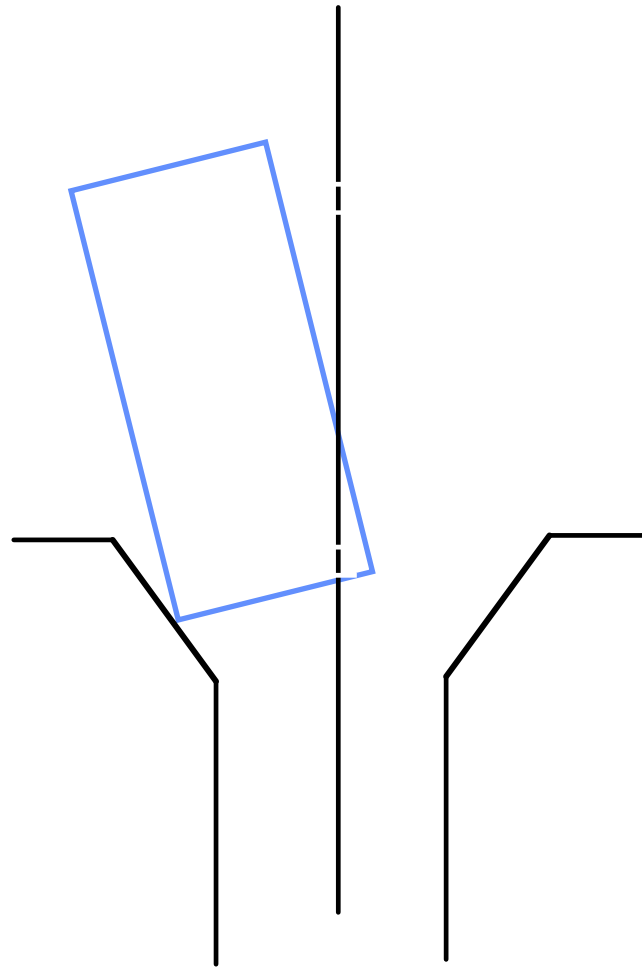
Insertion History



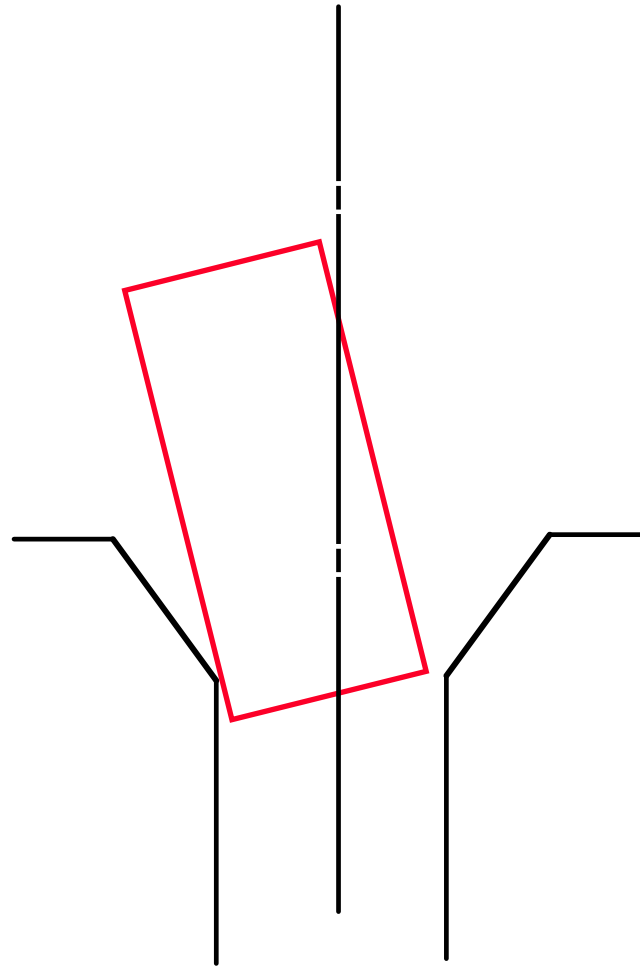
Insertion History



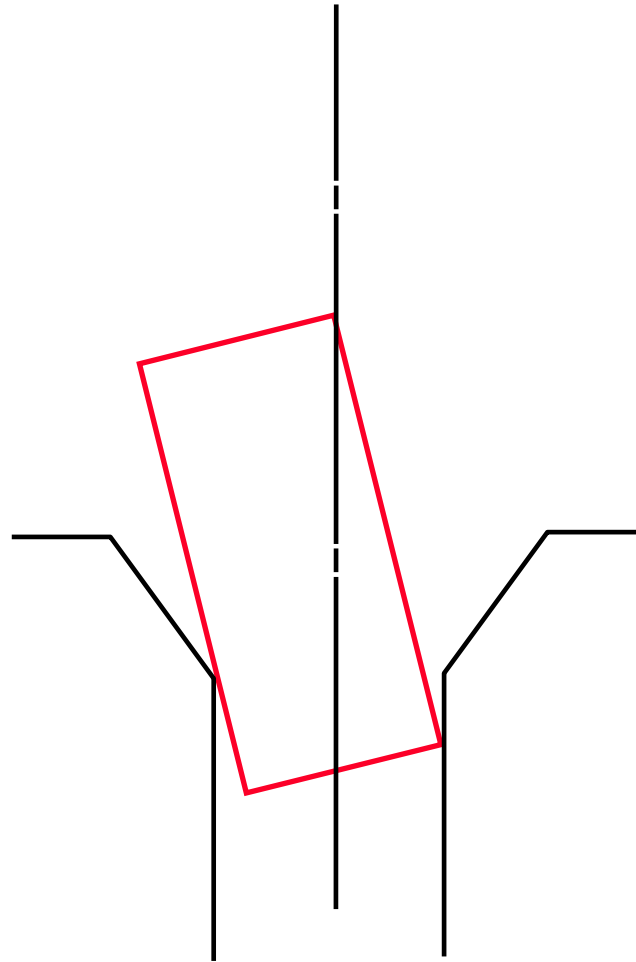
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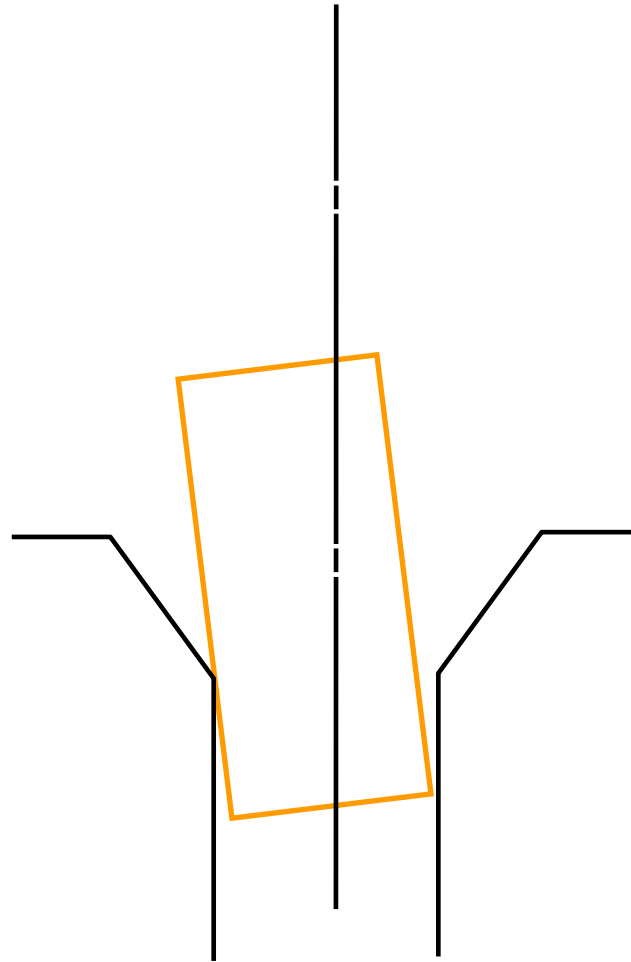
Insertion History



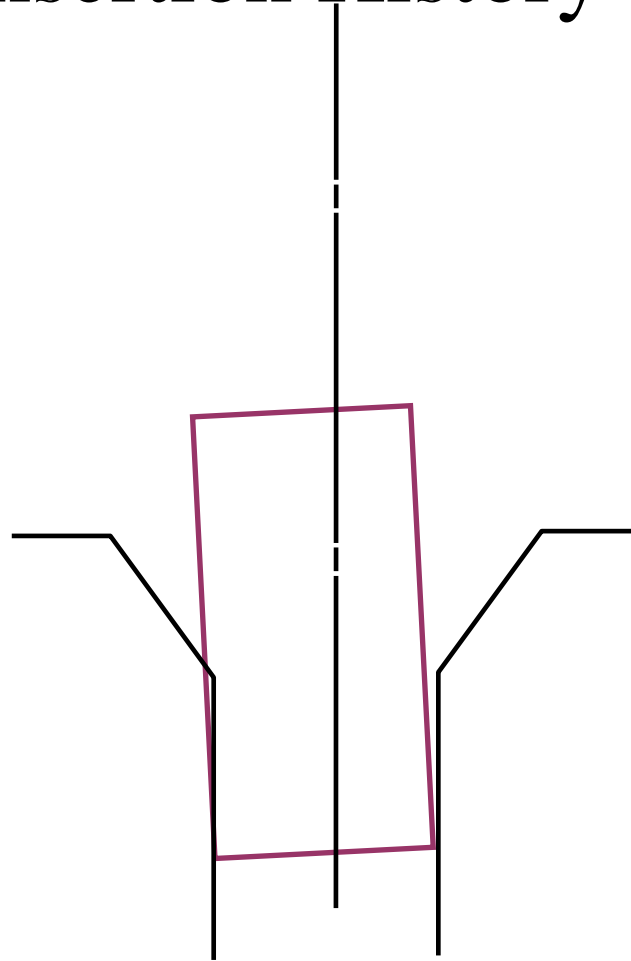
Insertion History



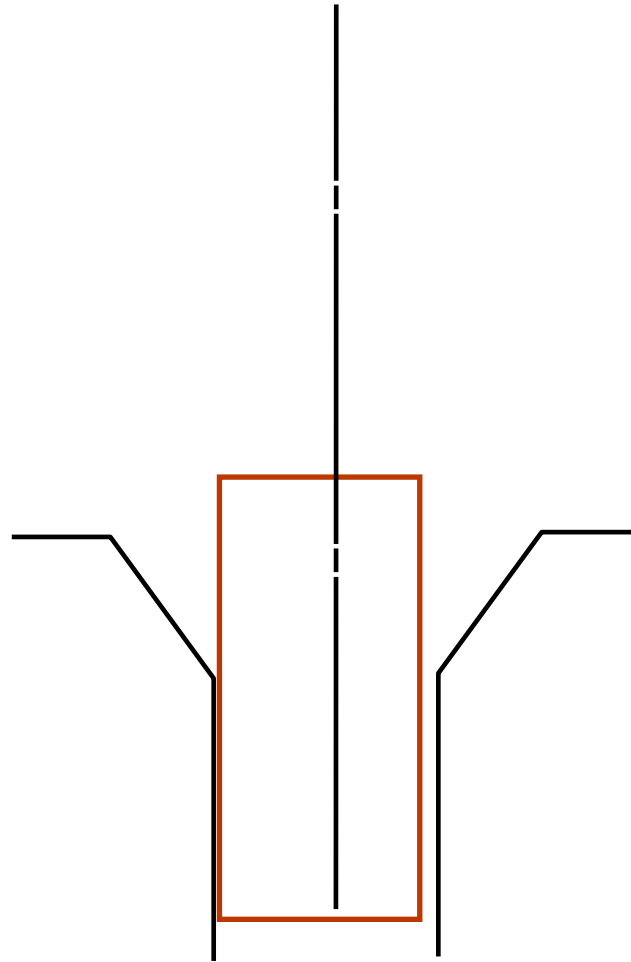
Insertion History



Insertion History



Insertion History



Life Cycle of a Part Mate

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Source:

Figure 10-12 in [Whitney 2004] Whitney, D. E. *Mechanical Assemblies: Their Design, Manufacture, and Role in Product Development*. New York, NY: Oxford University Press, 2004. ISBN: 0195157826.

Model of a Compliant Support

Images removed for copyright reasons.

Source:

Figure 10-10 in [Whitney 2004] Whitney, D. E.

*Mechanical Assemblies: Their Design, Manufacture,
and Role in Product Development.*

New York, NY: Oxford University Press, 2004. ISBN: 0195157826.

All support is assumed
concentrated at one point
and consists of one
lateral stiffness and one
angular stiffness

How Compliance Center Reacts to Force

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Source:

Figure 10-11 in [Whitney 2004] Whitney, D. E. *Mechanical Assemblies: Their Design, Manufacture, and Role in Product Development*. New York, NY: Oxford University Press, 2004. ISBN: 0195157826.

Force away from
C. C. causes rotation
and translation

Force on C. C. causes only translation

Forces and Moments - Two Point Contact Case

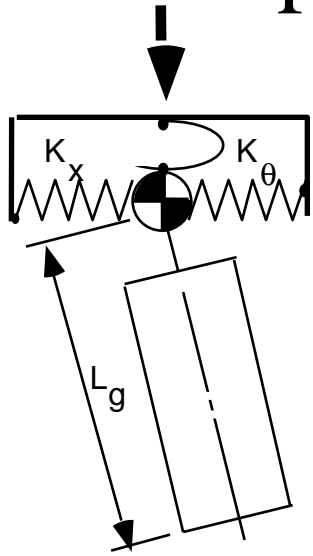
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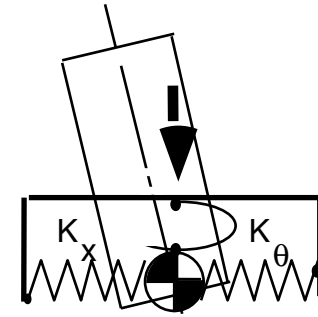
Figure 10-18 in [Whitney 2004] Whitney, D. E. *Mechanical Assemblies: Their Design, Manufacture, and Role in Product Development*. New York, NY: Oxford University Press, 2004. ISBN: 0195157826.

All applied and reaction
forces are expressed
in coordinates at peg's tip

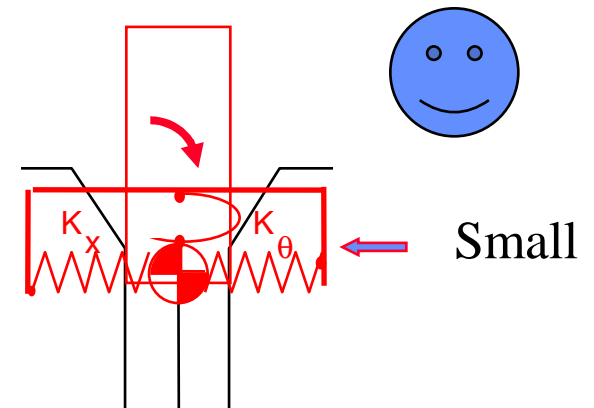
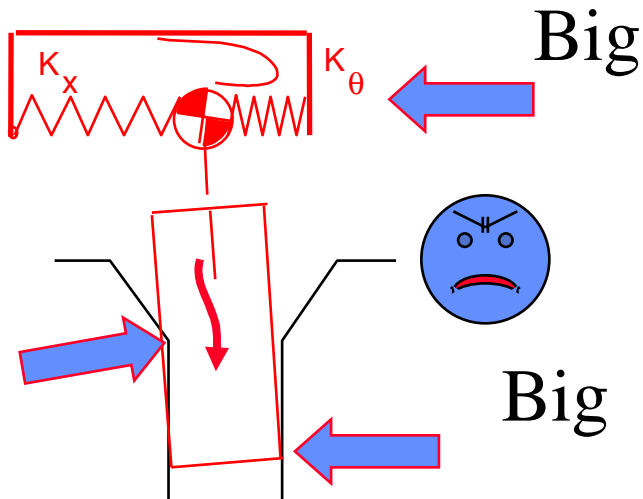
Forces Applied During Two-point Contact



When $L_g \gg 0$



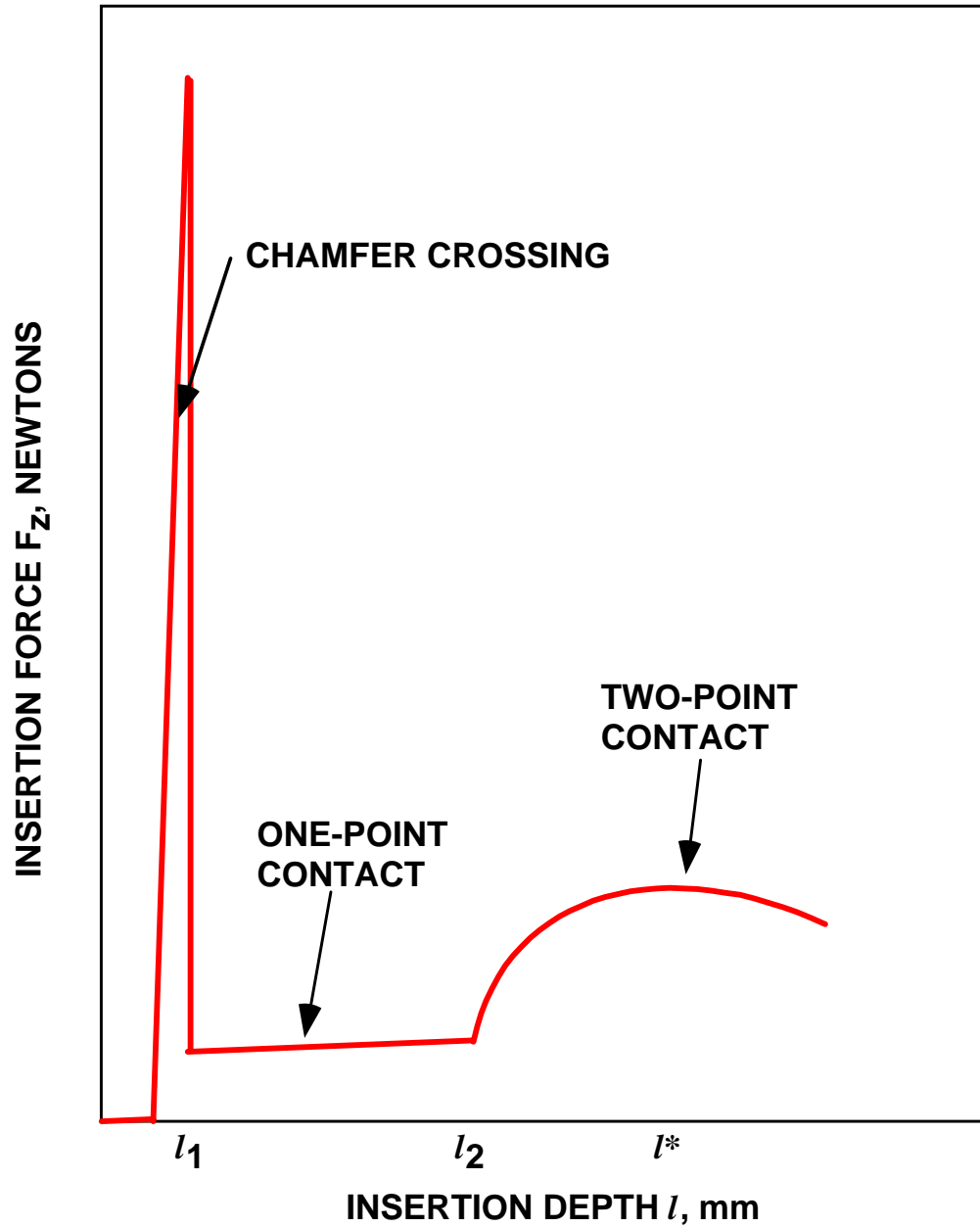
When $L_g \sim 0$



Making L_g Small is Good

- How to do it?
- Active Robot Force Feedback
 - Costly
 - Slow
- Some way that acts by itself
- It was invented almost 30 years ago
- Called Remote Center Compliance
- Reduces assembly force
- Avoids one of two main failure modes

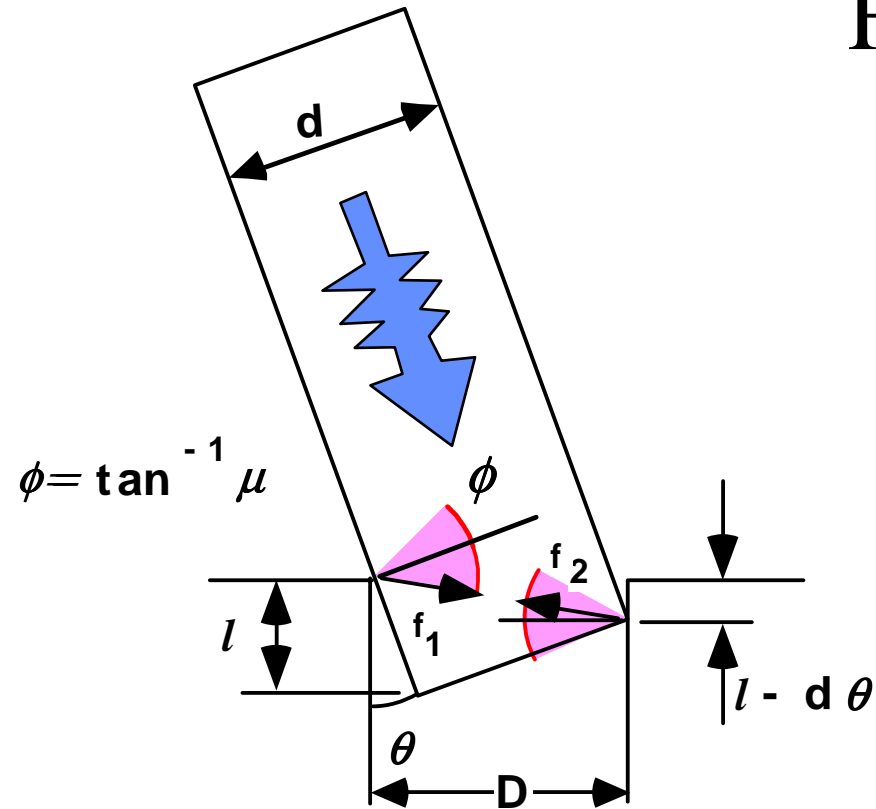
Insertion Force History



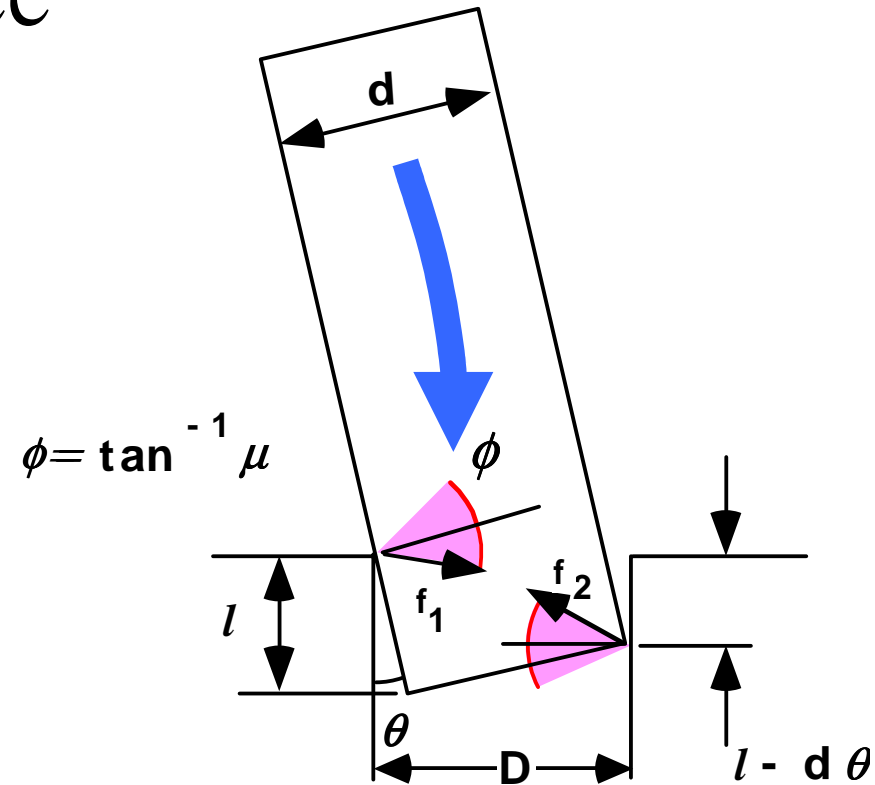
Assembly Failure Modes

- Both occur during two-point contact
- **Wedging** sets up compressive forces inside the parts
- **Jamming** results from incorrect insertion forces
- We can derive the requirements to avoid both of these failure modes

Wedging: Compressive Friction Forces Prevent Insertion Regardless of Insertion Force

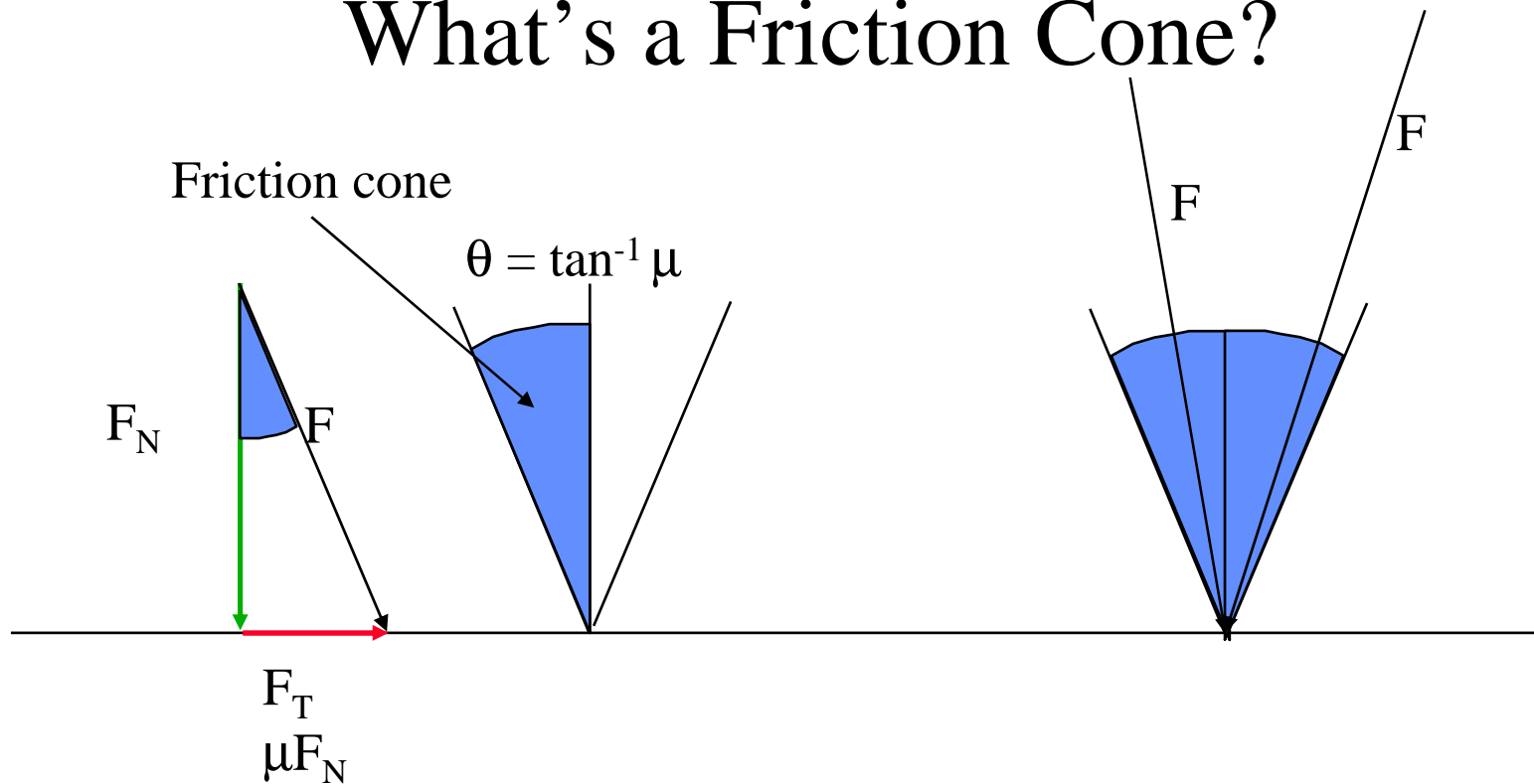


Wedging can happen if $\theta > c/\mu$ when two-point contact occurs



Wedging can be avoided if μ is small enough or if two-point contact occurs deep enough in the hole

What's a Friction Cone?



Sliding will occur if $F_T > \mu F_N$

$$F_T / F_N = \tan \theta$$

So, sliding will occur if $\tan \theta > \mu$

and F will lie on the boundary of the cone

If F is inside the cone then sliding will not happen because $F_T < \mu F_N$ and F can be *any* value

Conditions for Avoiding Wedging

$$S = \frac{L_g}{L_g^2 + K_\theta / K_x}$$

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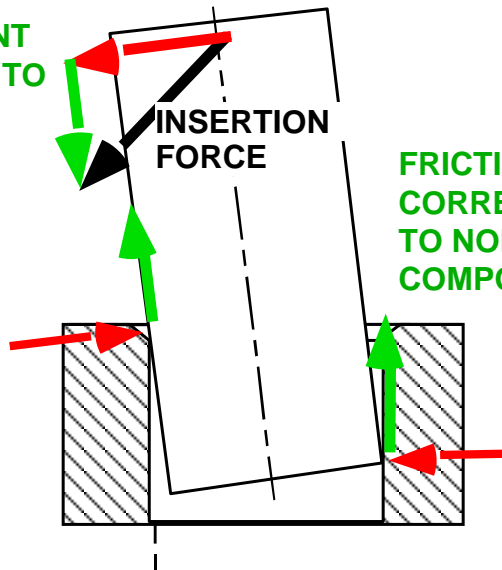
Source:

Figure 10-20 in [Whitney 2004] Whitney, D. E. *Mechanical Assemblies: Their Design, Manufacture, and Role in Product Development*. New York, NY: Oxford University Press, 2004. ISBN: 0195157826.

Jamming: Insertion Force Directed the Wrong Way - Can't Overcome Friction

COMPONENT NORMAL TO PEG AXIS

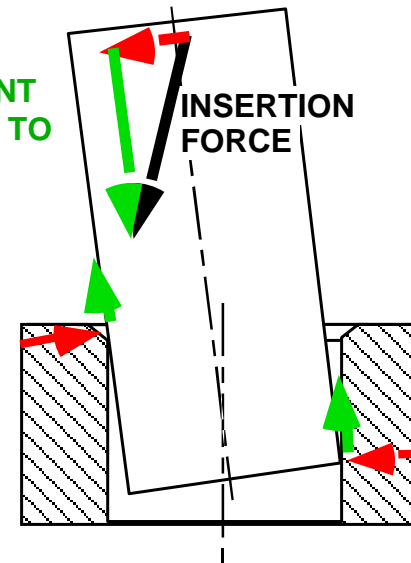
COMPONENT
PARALLEL TO
PEG AXIS



Component of
Insertion force
Along insertion direction
Not big enough:
Peg Is Jammed

COMPONENT NORMAL TO PEG AXIS

COMPONENT
PARALLEL TO
PEG AXIS



Component of
Insertion force
Along insertion direction
Is big enough:
Peg Goes In

Conditions for Avoiding Jamming

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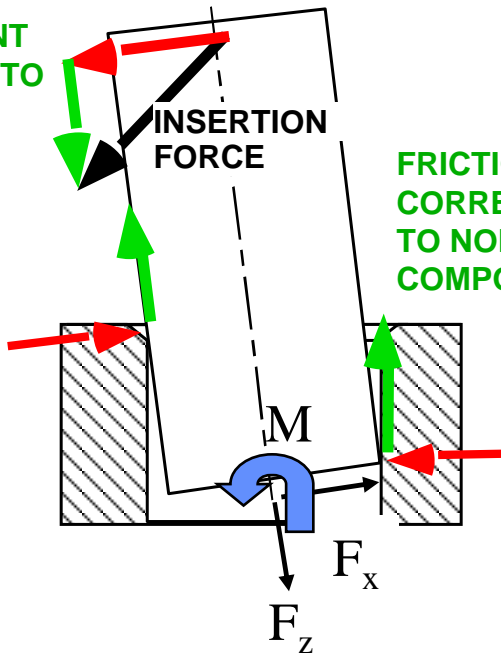
Source:

Figure 10-21 in [Whitney 2004] Whitney, D. E. *Mechanical Assemblies: Their Design, Manufacture, and Role in Product Development*. New York, NY: Oxford University Press, 2004. ISBN: 0195157826.

Jamming Examples

COMPONENT NORMAL TO PEG AXIS

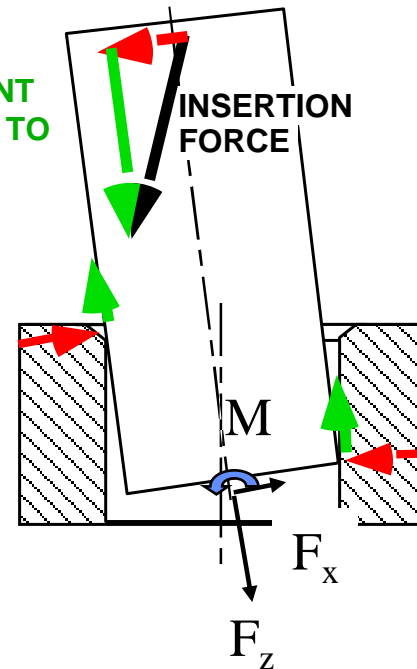
COMPONENT
PARALLEL TO
PEG AXIS



F_x/F_z is big.
 M/rF_z is big.

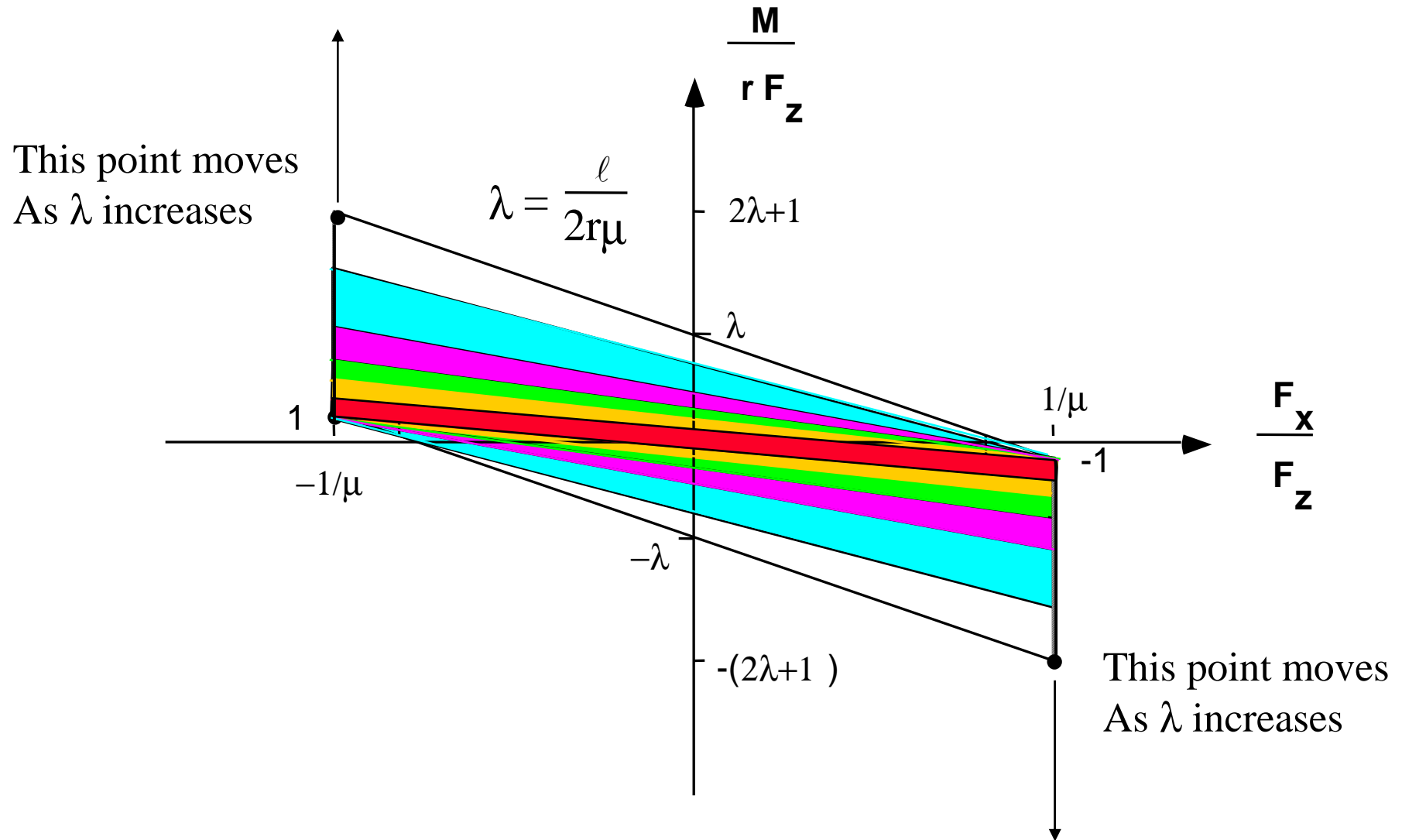
COMPONENT NORMAL TO PEG AXIS

COMPONENT
PARALLEL TO
PEG AXIS

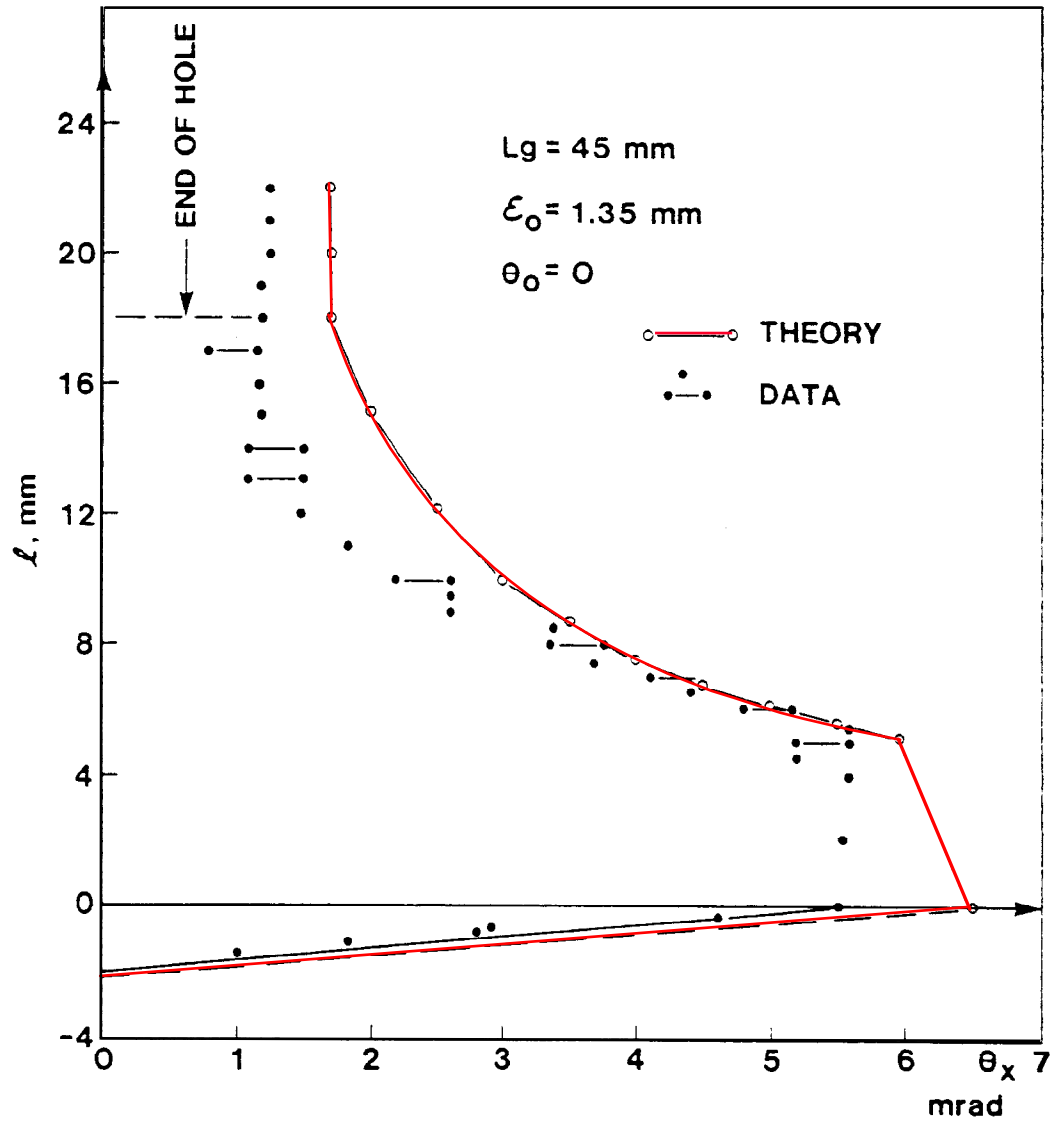


F_x/F_z is small.
 M/rF_z is small.

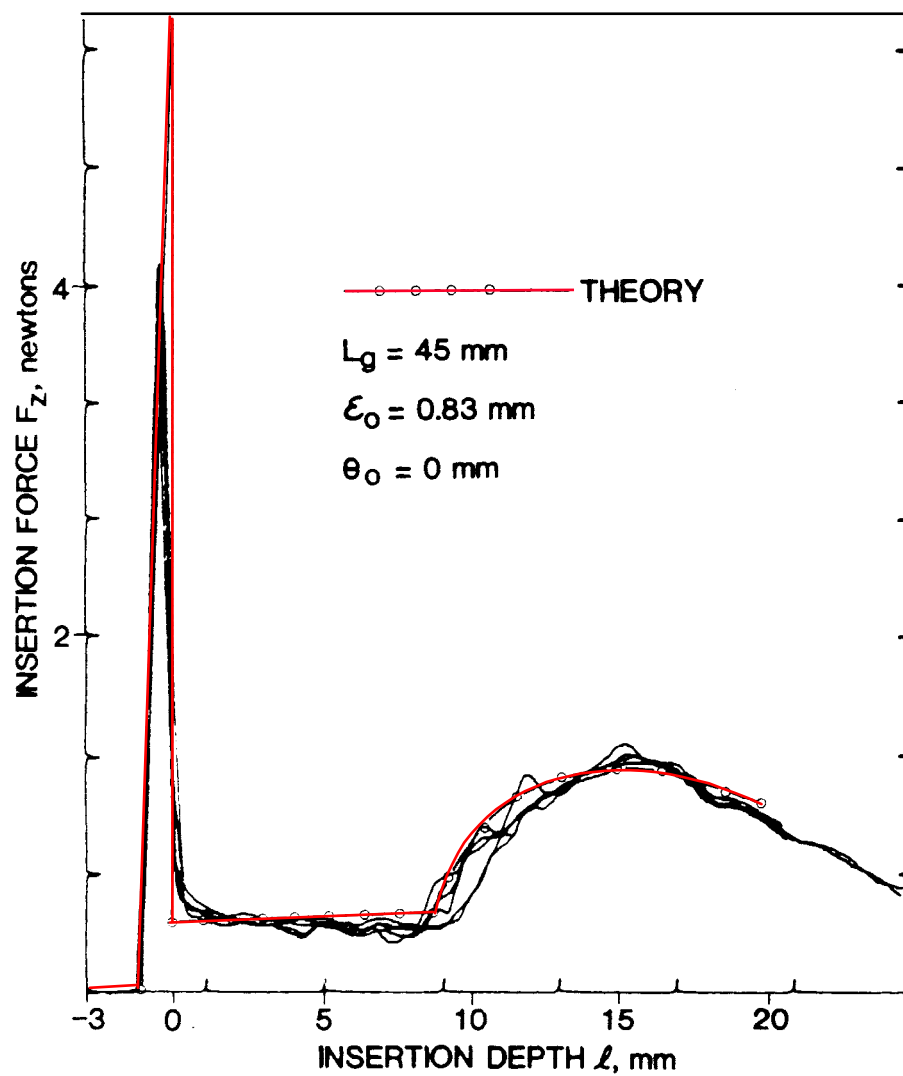
Target Expands as Depth Increases



Experimental Data



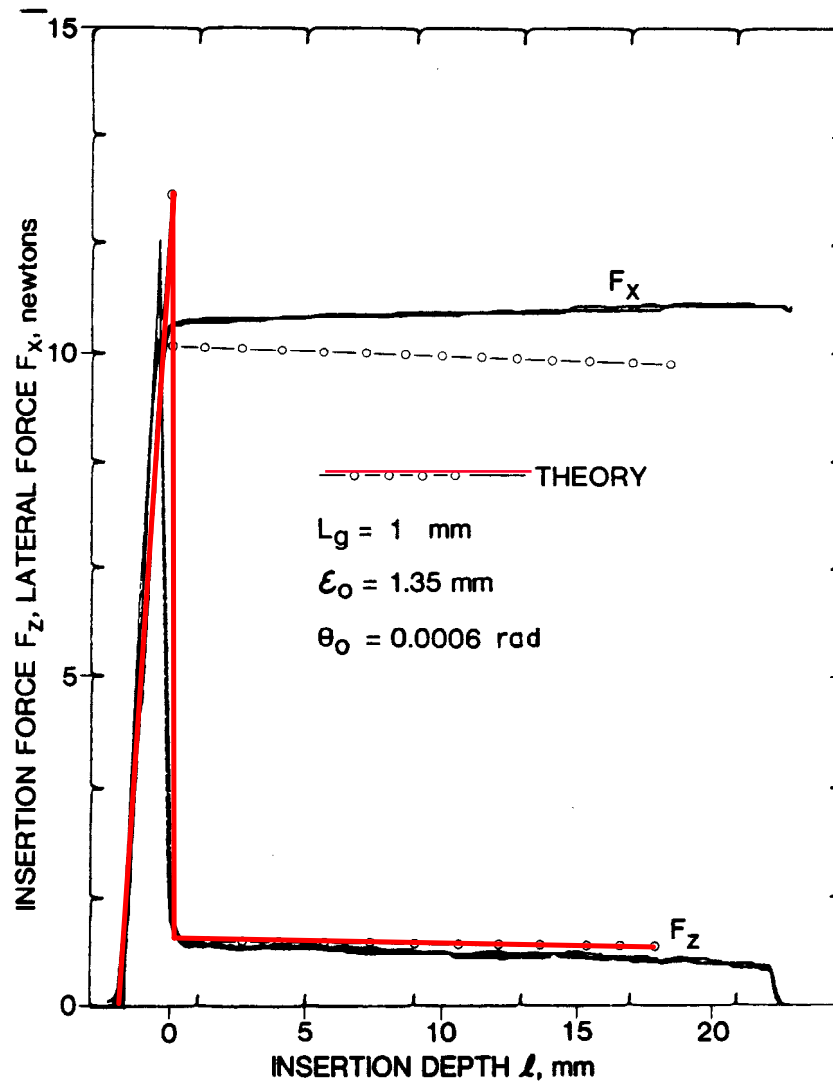
Experimental Data -2



Test Your Understanding

- Why does insertion force rise and then fall during two-point contact?

Experimental Data - 3



When $L_g = 0$ there is barely any insertion force. All that's left is chamfer crossing force.

Test Your Understanding Again

- Why does the insertion force not rise after chamfer-crossing is finished?

Review of Force Feedback Strategy

- Create a coordinate frame at the “working point” of the part or tool
- Separate lateral and angular sensing and response motions in that frame
- Devise a response strategy
- The Remote Center Compliance is a purely passive implementation of one such strategy

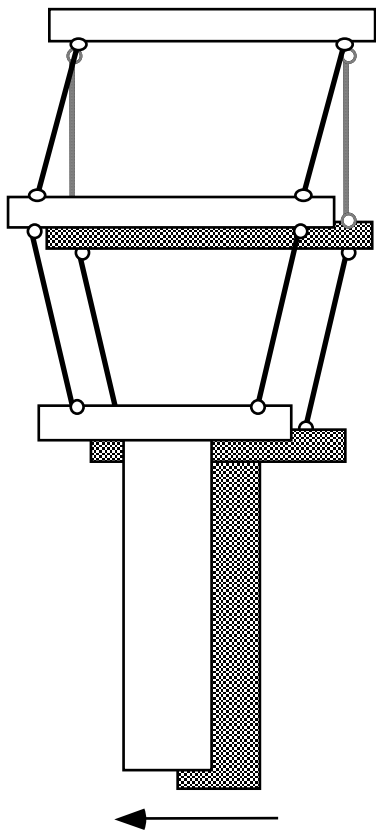
Simplified Explanation of the Remote Center Compliance (RCC)

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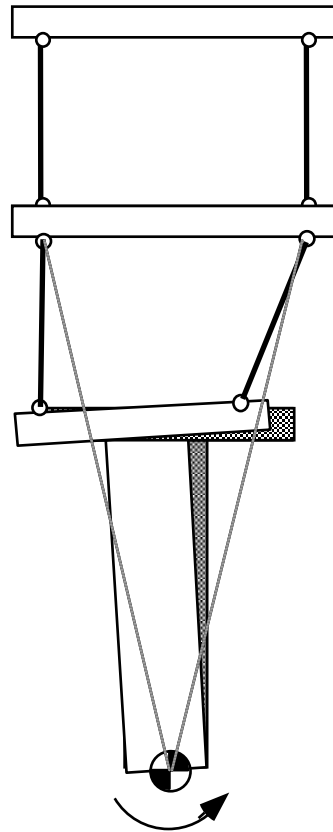
Source:

Figure 9-8 in [Whitney 2004] Whitney, D. E. *Mechanical Assemblies: Their Design, Manufacture, and Role in Product Development*. New York, NY: Oxford University Press, 2004. ISBN: 0195157826.

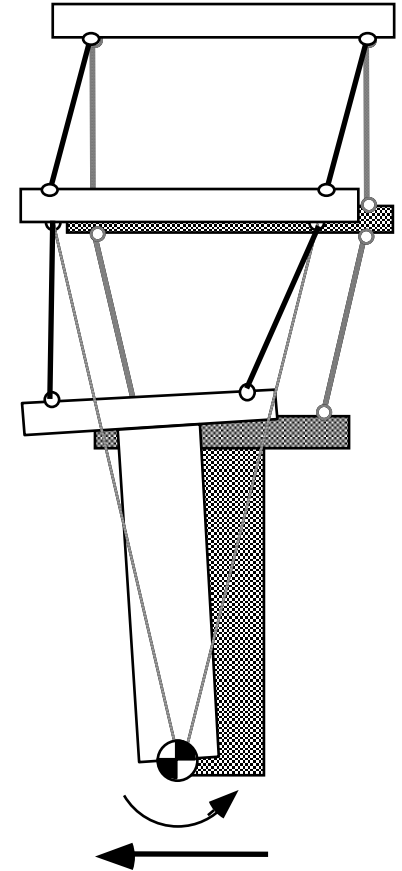
RCC Response to External Loads



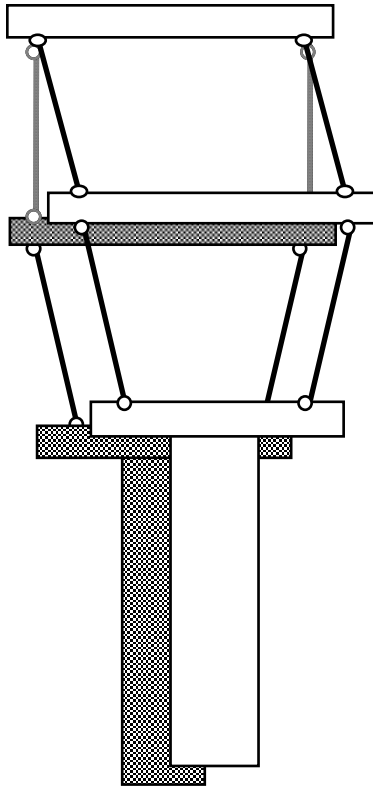
**(d) RCC UNDER
LATERAL LOAD**



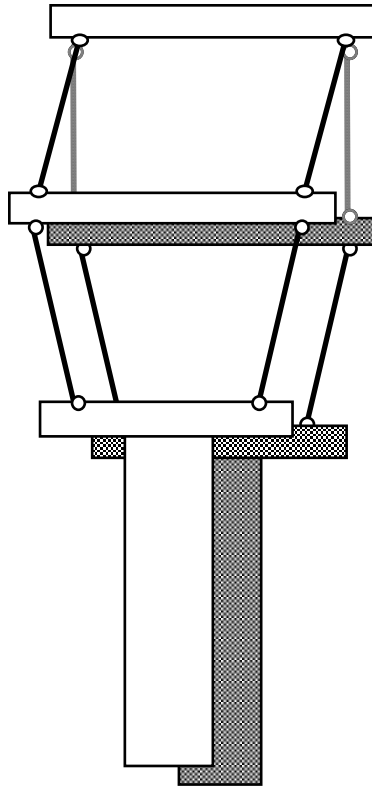
**(e) RCC UNDER
ANGULAR LOAD**



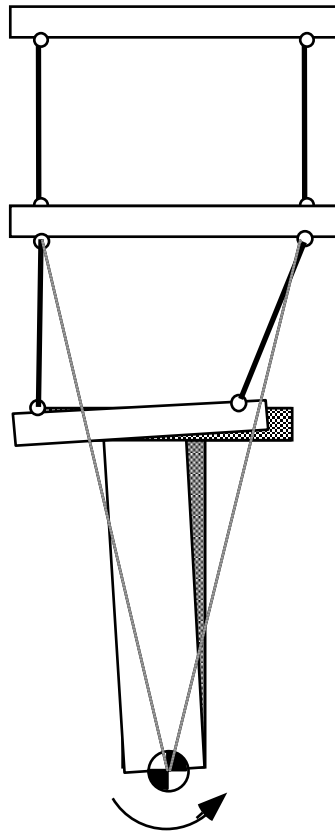
**(f) LINKAGE
RCC UNDER LATERAL
AND ANGULAR
DEFORMATION**



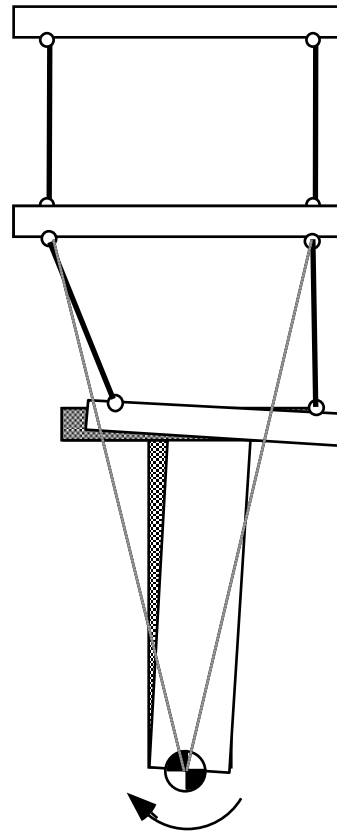
(d) RCC UNDER LATERAL LOAD



**(d) RCC UNDER
LATERAL LOAD**

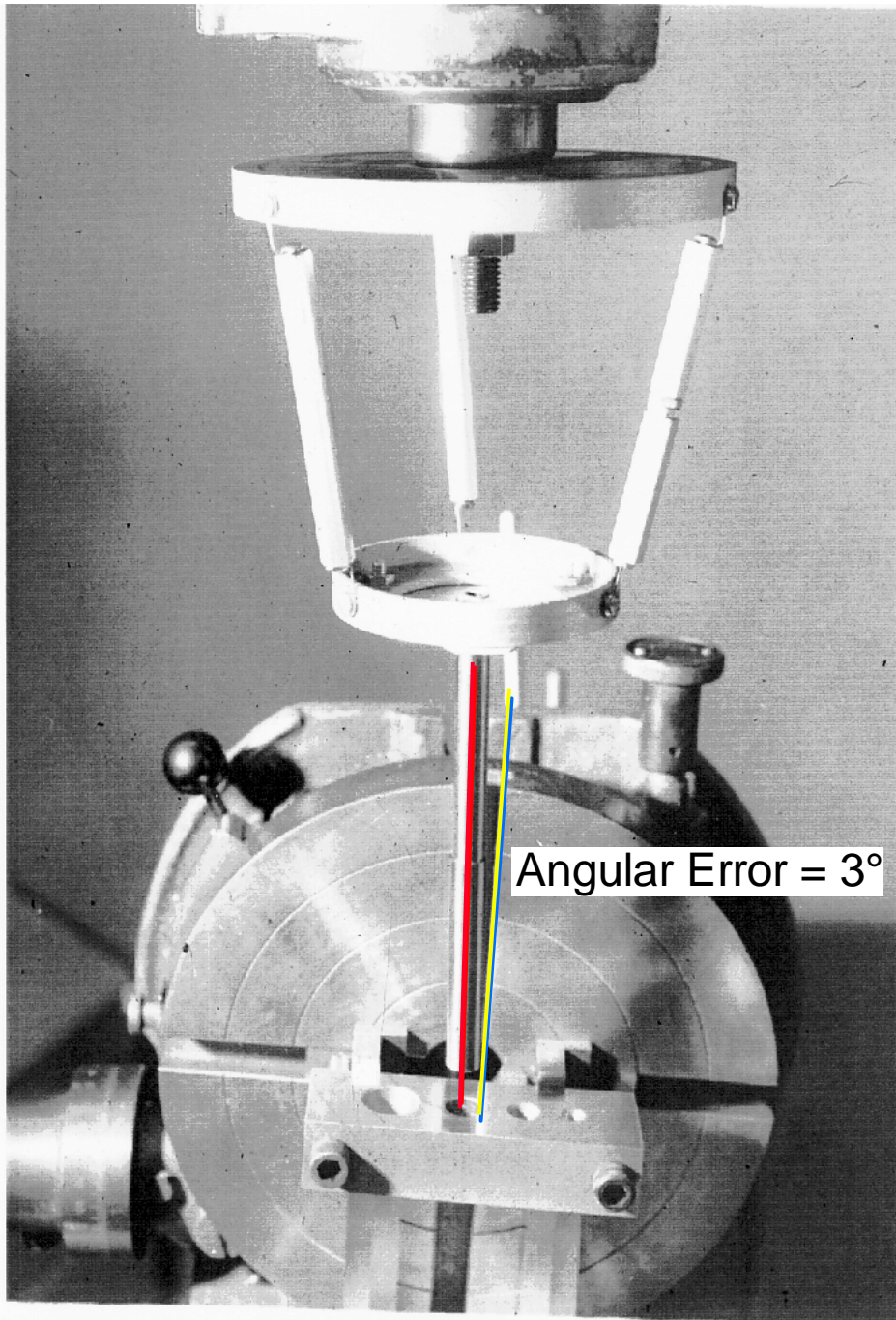


**(e) RCC UNDER
ANGULAR LOAD**



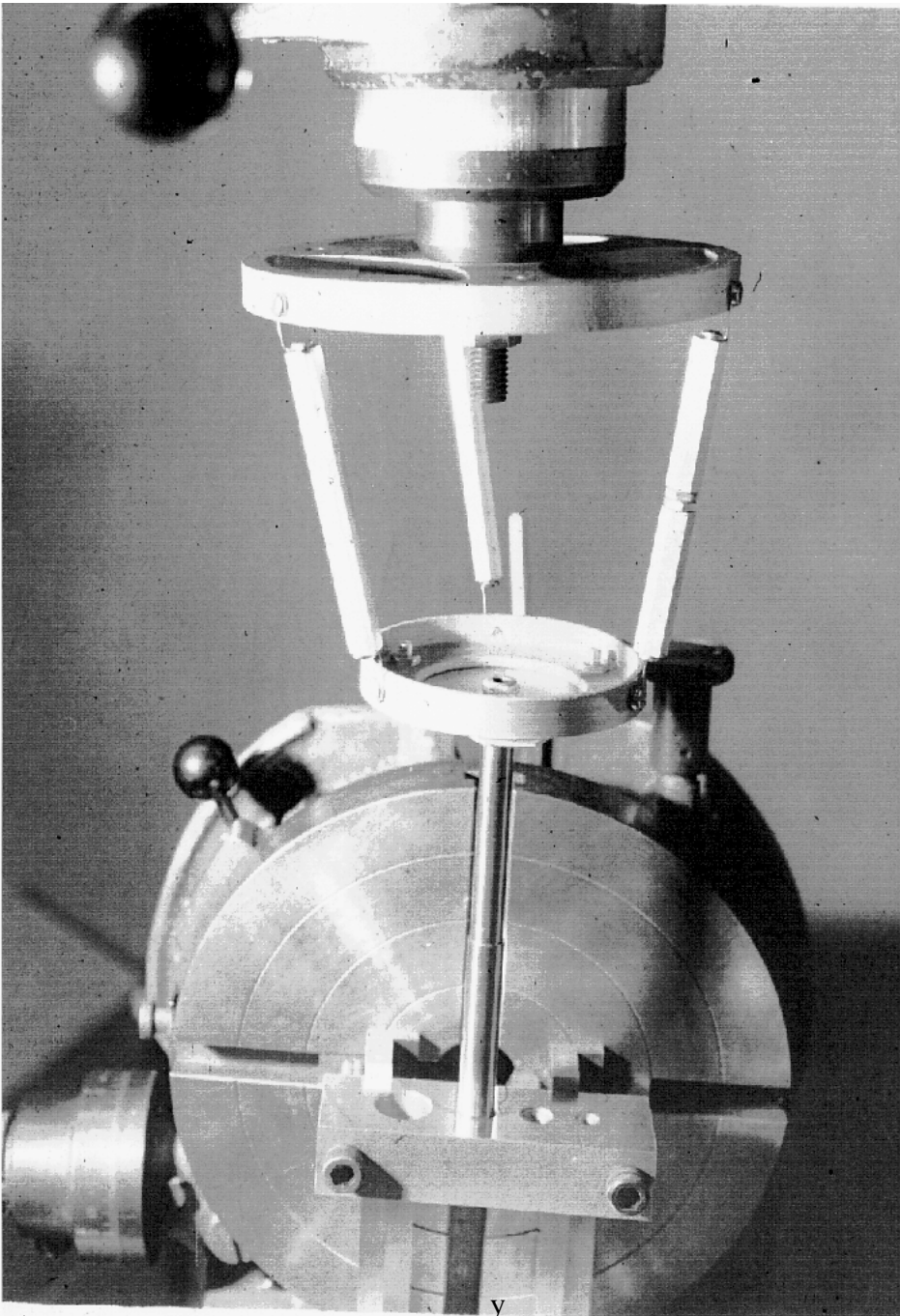
**(e) RCC UNDER
ANGULAR LOAD**

First RCC Experiment - 1



rigid part mating

First RCC Experiment - 2



rigid part mating

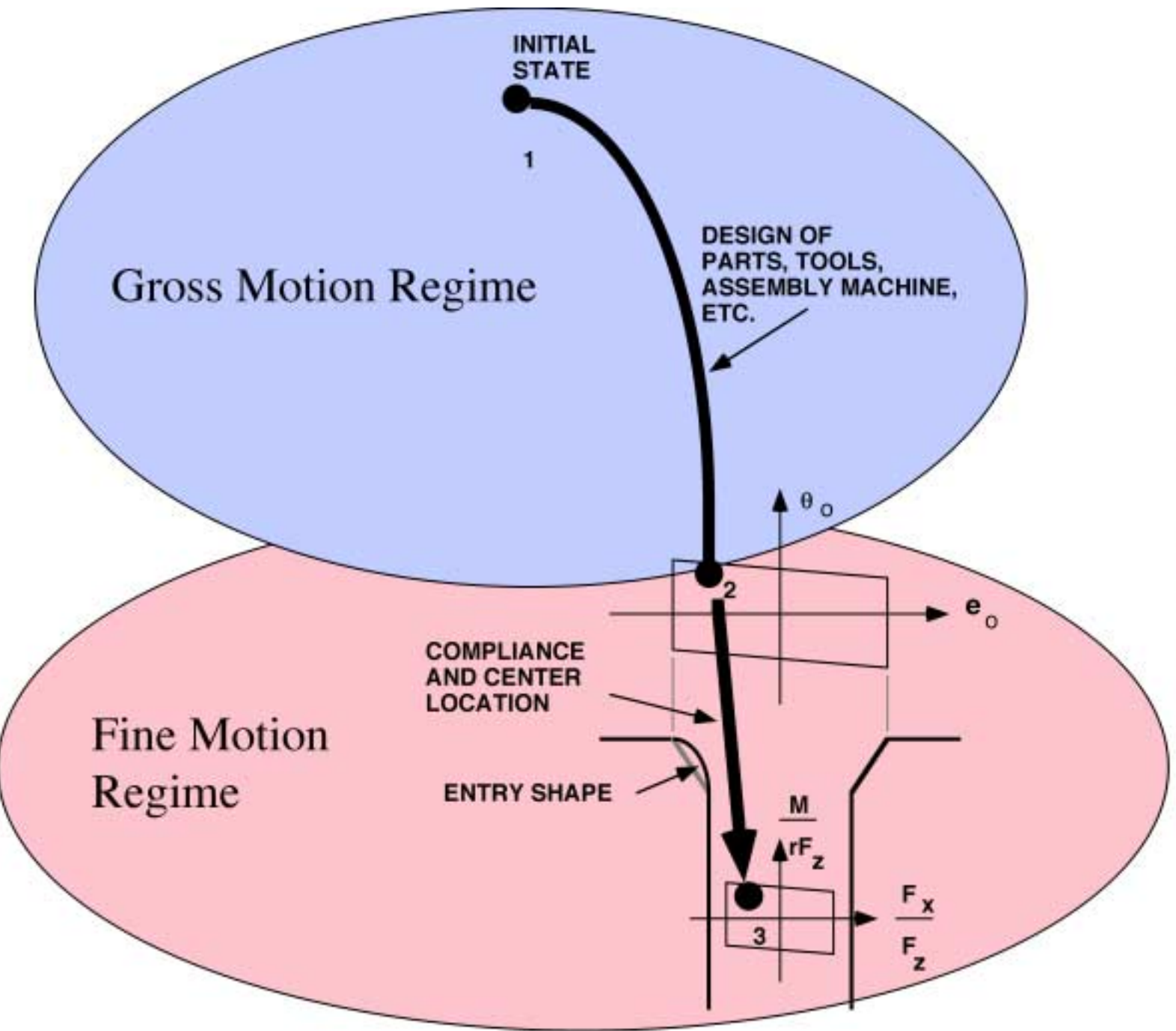
Commercial Remote Center Compliances

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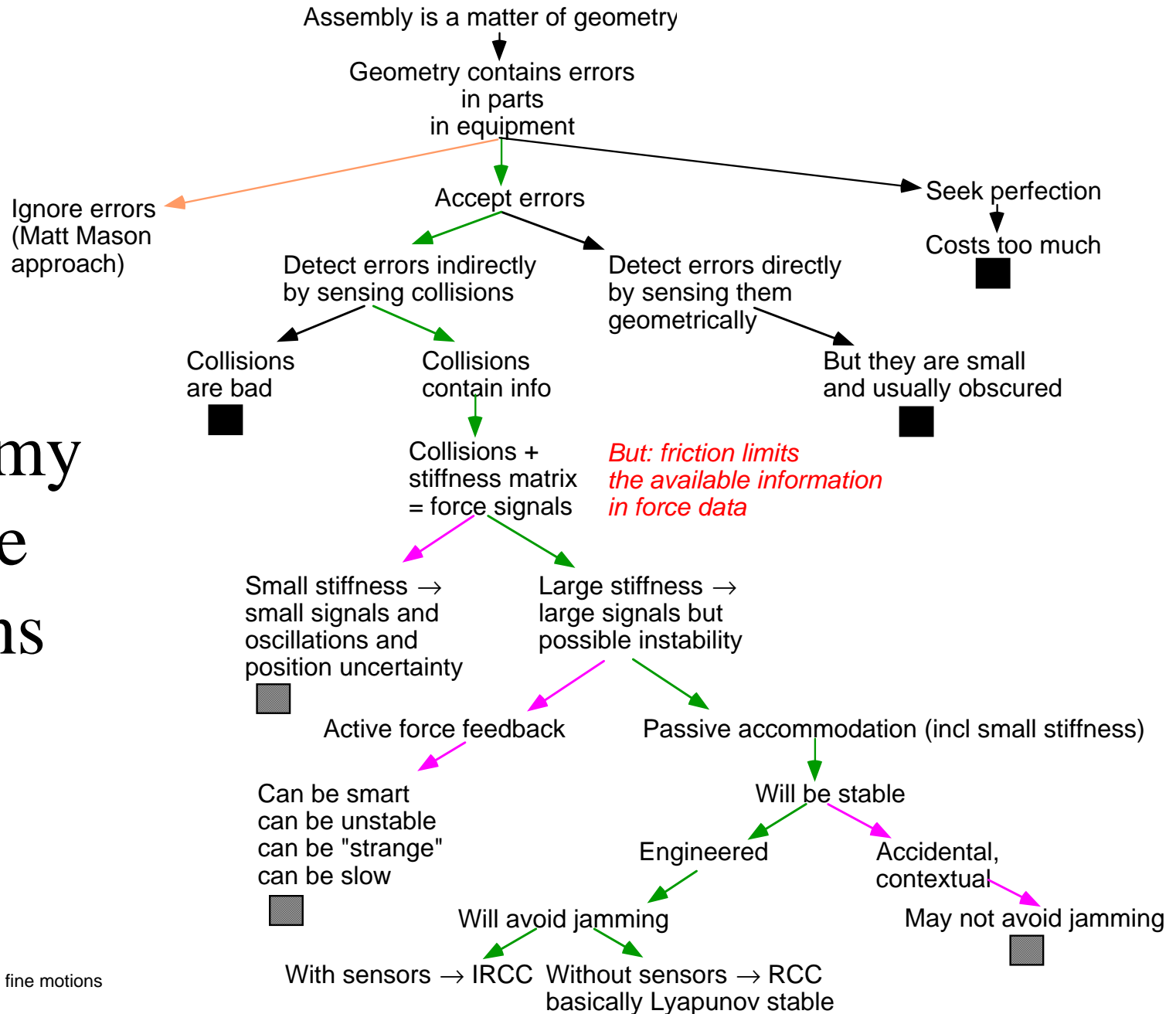
Source:

Figure 9-9 in [Whitney 2004] Whitney, D. E. *Mechanical Assemblies: Their Design, Manufacture, and Role in Product Development*. New York, NY: Oxford University Press, 2004. ISBN: 0195157826.

Compliant Assembly Strategy: Decouples Robot Accuracy from Task Precision



Taxonomy of Fine Motions



taxonomy of fine motions