2.830J / 6.780J / ESD.63J Control of Manufacturing Processes (SMA 6303) Spring 2008

For information about citing these materials or our Terms of Use, visit: http://ocw.mit.edu/terms.

Control of Manufacturing Processes

Subject 2.830/6.780 Subject 2.830/6.780 Spring 2008 Spring 2008 Lecture #3 "Process Variation – Physical Causes "Process Variation – Physical Causes and Interpreting Data" and Interpreting Data"

February 12, 2008 February 12, 2008

Agenda

- Process Definitions
	- Geometry Change Causality
- Taxonomy for Control
	- Classification of Change Methods
- "Mechanical" Examples
	- Turning
	- –Bending
	- –Molding
- Origins of Variation
	- –States and Properties

Process Model for Control

Back to the Process: What Causes the Output Change?

• A Directed Energy Exchange with the Equipment

Modes of Geometry Change?

- **Removal** of Material
- Plastic **Deformation** of Material
- **Addition** of Material
- **Formation** of Material from a Gas or Liquid
- Any others???

What Controls the Geometry Change?

Location and Intensity of Energy Exchange

• Examples:

–– location of max. shear stress in turning

What Controls the Geometry Change?

Location and Intensity of Energy Exchange

- Examples:
	- heat transfer at the mold surface in injection molding

Control of Geometry Change?

Location and Intensity of Energy Exchange

• Examples:

– location of laser beam in laser cutting

Control of Geometry Change?

Location and Intensity of Energy Exchange

and the state of the – reaction rate - time product on substrate surface $\:$ in LPCVD

Control of Geometry Change?

Location and Intensity of Energy Exchange

• displacement field in sheet forming :

Two Extremes of Interactions

Area of E(t) << Total Area: Serial Process

Area of $E(t)$ ~ Total Area: Parallel Process

Two Extremes of Interactions

- Concentrated, "Lumped" Energy Port –Small Area Wrt Total Part Geometry
- Distributed Energy Port
	- –Area ~ Total Part Geometry

What Determines Part Geometry Change?

- For Lumped case:
	- – time - trajectory of the port location
		- e.g. tool paths
- For Distributed Case:
	- Shape of the energy distribution
		- patterns
		- molds
		- masks

Examples

- Serial (Lumped) Processes
	- –Machining - Tool Path
	- Laser Cutting -
	- Bending
	- Stereolithography Beam Path
	- Three D Printing the Sinder Path
-
- Beam path
	- **Tool Depth**
		-

Examples

- Parallel (Distributed) Processes
	- –Draw Forming - Die Shapes
	-
	- Chemical Etching Mask Shape
	- CMP
	- Plating
-
- Injection Molding Mold Shape
	- - Tool Shape
		- **Substrate Shape**

Toward a Process Taxonomy

- Classify by Change Mode –Why?
- Classify by Intera _{Sensitivity, resolution} arallel) – So what?
- Classify by Energy Domain

– Who cares??

Flexibility, controllability, rate

Rate, resolution

Process Taxonomy for Control

Process Model for Control

Process Parameters

- Equipment Energy "States"
- Equipment Constitutive "Properties"
- Material Energy "States"
- Material Constitutive "Properties"

$$
\leftarrow \text{Equivalent} \leftarrow \text{Material} \rightarrow
$$

Energy States

$$
\leftarrow \text{Equivalent} \left\{\frac{\overline{E}(t)}{\text{Material}}\right\}
$$

Properties

- *Extensive*: GEOMETRY
- *Intensive*: Constitutive Properties
	- –Modulus of Elasticity, damping, mass
	- Plastic Flow Properties
	- Viscosity
	- Resistance, Inductance, Capacitance
	- Chemical Reactivity
	- Heat Transfer Coefficient

A Model for Process Variations

 \bullet Recall: $\underline{Y} = \Phi(\underline{\alpha})$

• One or more α*'s* "qualify" as inputs : *^u*

$$
\underline{Y} = \Phi(\underline{\alpha}, \underline{u});
$$
 $\underline{u} = \text{vector of inputs}$

• The first order Variation $\Delta \mathsf{Y}$ gives the "Variation $\;$ Equation"

Parallels From Lecture 2

Image removed due to copyright restrictions. Please see Fig. 26 in Boning, D. S., et al. "A General Semiconductor Process Modeling Framework." *IEEE Transactions on Semiconductor Manufacturing* 5 (November 1992): 266-280.

Simple Machining

- Process Type?
- Equipment States and Properties?
- Material States and Properties?

Sources of Variation?

Simple Machining (Orthogonal Turning

CNC Data

Average Values

2.830J/6.780J Lecture #3 \degree David E. Hardt 31

Manufacturing

Average Values

Machining: Conclusions

- Geometry Transformation is (In General) well behaved
	- Not highly sensitive to material property variations
	- New Surface Where Tool is Located
- Dominant Sources of Variation:
	- – Tool Positioning errors - Equipment Properties and States
- Feedback control of Positions is a good idea -> CNC control!

Brake Bending

Images removed due to copyright restrictions. Please see:

<http://www.falconfab.com/MVC-016F.JPG>

<http://www.falconfab.com/MVC-007F.JPG>

http://edevice.fujitsu.com/fj/DATASHEET/epk/fpt-100p-m20.pdf

Bending

- Process Type?
- Equipment States and Properties?
- Material States and Properties?

Simple Model : Pure Moment Bending

Constant Radius Tool

Simple Bending Mechanics: Parameter Effects

- Tool Shape $(\mathsf{R}_{\mathsf{tool}})$ determines the shape under load
- Elastic Springback determines the final shape
- What determines the springback?

Simple Bending Model

 $K =$ curvature of the tooling $h =$ thickness of the sheet $\varepsilon(y)$ = through thickness strain What is M(K) (or K(M)) ?

Simple Beam Theory

Elastic Perfectly Plastic Model

The M-K Curve

Final Shape: Springback

$$
\Delta K = \frac{M_{\max}}{EI} \cdot K_{part} = K_{\text{tool}} - \Delta K
$$

 $K =$ shape of tool

E= material property $I =$ 1 12bh³ *cubic* dependence on thickness

$$
M_{\text{max}} = ?
$$

$$
M_{\text{max}} = \Phi(K_{\text{Y}}, EI)
$$

Strong Dependence on yield properties

Effect of Material Variations: Increase in Yield Stress

Bending Experiments

- Bend to 2 different depths
- Two different materials
	- 0.028" Steel
	- 0.032" Aluminum

Steel vs. Aluminum

Bending by Operating Point

Other Possible Variations

- Yield Stress (<u>+ 10%reported)</u> –Chemistry, working history
- Thickness
	- –Rolling mill quality
	- Design vs. manufacturing specs
- Tooling Errors

Conclusions

- \bullet Some Variations Easily Explained
	- Deterministic parameter changes
		- Thickness and Material Selection \vartriangle m_p (Material Parameter)
	- Intentional Input changes
		- Depth changes $\varDelta \mathbf{e}_{\mathrm{s}}$ (Equipment state)
- \bullet Other Variations ???
	- Property Variations within Material Δm_{p}
	- Machine Errors $\Delta \mathbf{e}_{\mathsf{p}}$ and $\Delta \mathbf{e}_{\mathsf{s}}$ (e.g. deflection and position error)

$$
\Delta Y = \frac{\partial Y}{\partial \alpha} \Delta \alpha + \frac{\partial Y}{\partial u} \Delta u
$$

Conclusions for Brake Bending

- Equipment Errors have Strong Effect on Final Shape
	- Punch Penetration
		- Die Width

 $\rightarrow \Delta e_s$ (Equipment state)

- ->-> Δe_{p} (Equipment Parameter)
- **SO WHAT? Large ∂Y/∂**^α **Large** Δα

Injection Molding

Injection Molding Process

Process Type?

Equipment States and Properties?

Material States and Properties?

Geometry Determinants

- Mold Shape
- Material Shape Change upon **Cooling**
	- Residual Stress Effect
	- Thermal Expansion or contraction
- Extent of Mold Filling

 $P = R(v) Q$

Manufacturing

Effect of Temperature on Flow

 $Q = P/R$ R = resistance to flow α v $v(T) = Ae^{ER(T_0-T)}$

where:

- T = temperature
- $R = gas constant$
- $E =$ activation energy for viscosity

Key Material Properties: **Cooling**

Packing Phase

Heat Transfer: Filling

- $\mathsf{T}_{\mathsf{part}}$ > $\mathsf{T}_{\mathsf{mod}}$ therefore always cooling
- Interior hotter than surface
- If $\mathsf{T}_{\mathsf{part}}$ on surface $<\mathsf{T}_{\mathsf{g}}$ flow stops – Short Shot
- Viscosity is strong function of Temperature

Heat Transfer in the Mold

- q = k A ∂T/∂^x
	- Rate decreases as ∂T/∂x decreases
		- Mold heat & polymer cools
- dT/dt = α ∂T²/∂x²
	- α = k / β C_p
		- Polymers have low k and high Cp

Process Control Issues

- Control Change in Shape upon Cooling
	- –Consistent Mold Filling
	- Consistent Mold Pressure
		- Consistent Residual Stresses
	- Consistent Thermal environment
		- Consistent Thermal Distortion

Typical Equipment Control Systems

- Injection Velocity or Injection Pressure
- Nozzle Temperature
- Mold Temperature
- Barrel Heater Temperature

Equipment States

Sources of Variation

- Material Properties
	- Flow Properties
		- ^ν(T) relationship (especially if moist)
	- –Thermal properties (ditto)
	- Also effects of "regrind"

Example: Effect of Blending

Figure by MIT OpenCourseWare.

Lab Data

- Variable Hold Time
- Variable Injection **Velocity**

Injection Molding Data

Injection Molding NTU

I.M. NTU (no Group 1)

Sources of Variation

- Equipment Properties
	- –Heat Transfer Properties
	- Mold Flow Passages
- Equipment States
	- Barrel and Nozzle Temperatures
	- Mold Temperatures
	- Flow Rates
	- Packing Pressure

Conclusions

- I.M. is a Complex, Parallel Formation Process
- Strong Dependence on Material Properties
	- Viscosity sensitivity
	- Heat Transfer Sensitivity
- Thermal State Must be Well Controlled
	- Many opportunities on the equipment
	- Material State very hard to do
		- Distributed
		- Interference with Process

Conclusions: Variation

 $\Delta \alpha$ + $\frac{\partial Y}{\partial x}$

∂*^u*

Δ*u*

Disturbances

 $\Delta Y =$

 $Y = \frac{\partial Y}{\partial Y}$

∂α

Control Inputs: Equipment States

Equipment Property Changes Material Property Changes Material State Uncertainty Equipment State Uncertainty

Process Model for Control

What *are* the *Process Parameters*?

- Equipment Energy "States"
- Equipment Constitutive "Properties"
- Material Energy "States"
- Material Constitutive "Properties"

Energy States

Properties

- *Extensive*: GEOMETRY
- *Intensive*: Constitutive Properties
	- –Modulus of Elasticity, damping, mass
	- Plastic Flow Properties
	- Viscosity
	- Resistance, Inductance, Capacitance
	- Chemical Reactivity
	- Heat Transfer Coefficient
- \bullet Which has the highest precision?

A Model for Process Variations

\n- Recall:
\n- $$
\underline{Y} = \Phi(\underline{\alpha})
$$
\n

•One or more α*'s* "qualify" as inputs : *^u*

$$
\underline{Y} = \Phi(\underline{\alpha}, \underline{u});
$$
 $\underline{u} = \text{vector of inputs}$

•The first order Variation ΔY gives the "Variation Equation"

The Variation Equation

Disturbances

Primary Process Control Goal: Minimize $\Delta\mathsf{Y}$

How do we make Δ*Y* → ? 0

$$
\Delta Y = \frac{\partial Y}{\partial \alpha} \Delta \alpha + \frac{\partial Y}{\partial u} \Delta u
$$

- \bullet hold *u* fixed (Δ*^u* = 0)
	- –operator training (SOP's)
	- –good steady-state machine physics
- \bullet minimize disturbances

 \Box Δα ->Δα_{min}

This is the goal of Statistical Process Control (SPC)

OR

$$
\Delta Y = \frac{\partial Y}{\partial \alpha} \Delta \alpha + \frac{\partial Y}{\partial u} \Delta u \qquad \Delta Y \to 0
$$

- hold u fixed (Δ*^u* = 0)
- minimize the term: $\tilde{\rightarrow}$ the disturbance sensitivity ∂*Y* $\partial \alpha$

This is the goal of Process Optimization This is the goal of Process Optimization

$$
\text{Assuming } \frac{\partial Y}{\partial \alpha} = \Phi(\underline{\alpha}) \quad \underline{\alpha} = \text{operating point}
$$

OR

$$
\Delta Y = \frac{\partial Y}{\partial \alpha} \Delta \alpha + \frac{\partial Y}{\partial u} \Delta u \qquad \Delta Y \to 0
$$

•manipulate Δ*^u by measuring* Δ*Y such that*

$$
\Delta u \frac{\partial Y}{\partial u} = -\frac{\partial Y}{\partial \alpha} \Delta \alpha
$$

This is the goal of Process Feedback Control This is the goal of Process Feedback Control

•Compensating for (not eliminating) disturbances

Statistical Process Control

Process Optimization

Output Feedback Control

Compensate for Disturbances

Process Control Hierarchy

• Reduce Disturbances

- Good Housekeeping
- Standard Operations (SOP's)
- **Statistical Analysis and Identification of Sources (SPC)**
- **Feedback Control of Machines**
- Reduce Sensitivity (increase "Robustness")
	- **Measure Sensitivities via Designed Experiments**
	- Adjust "free" parameters to minimize
- Measure output and manipulate inputs
	- **Feedback control of Output(s)**

