

2.092/2.093

FINITE ELEMENT ANALYSIS OF SOLIDS AND FLUIDS I

FALL 2009

Quiz #2-solution

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Problem 1 (10 points):

$$h_i^s = \frac{1}{4} \left(1 - \frac{x}{2}\right) (1 - y); \quad h_i^f = \frac{1}{4} \left(1 - \frac{x}{2}\right) \left(1 + \frac{y}{2}\right).$$

$$h_{i,x}^s = -\frac{1}{8} (1 - y); \quad h_{i,y}^s = -\frac{1}{4} \left(1 - \frac{x}{2}\right).$$

$$h_{i,x}^f = -\frac{1}{8} \left(1 + \frac{y}{2}\right); \quad h_{i,y}^f = \frac{1}{8} \left(1 - \frac{x}{2}\right)$$

$$\underline{\mathbf{H}}^{(1)} = \begin{bmatrix} h_i^s & 0 \\ 0 & h_i^s \end{bmatrix}; \quad \underline{\mathbf{H}}^{(2)} = \begin{bmatrix} h_i^f & 0 \\ 0 & h_i^f \end{bmatrix}.$$

$$\underline{\mathbf{U}}^T = [u_i \quad v_i].$$

$$\underline{\mathbf{B}}^{(1)} = \begin{bmatrix} h_{i,x}^s & 0 \\ 0 & h_{i,y}^s \\ h_{i,y}^s & h_{i,x}^s \end{bmatrix}; \quad \underline{\mathbf{B}}^{(2)} = [h_{i,x}^f \quad h_{i,y}^f].$$

$$\underline{\mathbf{M}}^{(1)} = \int_{V^{(1)}} \rho_s \underline{\mathbf{H}}^{(1)T} \underline{\mathbf{H}}^{(1)} dV^{(1)} = \rho_s \int_{-1}^1 \int_{-2}^2 \underline{\mathbf{H}}^{(1)T} \underline{\mathbf{H}}^{(1)} dx dy$$

$$\underline{\underline{M}}^{(2)} = \int_{V^{(2)}} \rho_f \underline{\underline{H}}^{(2)T} \underline{\underline{H}}^{(2)} dV^{(2)} = \rho_f \int_{-2}^2 \int_{-2}^2 \underline{\underline{H}}^{(2)T} \underline{\underline{H}}^{(2)} dx dy$$

$$\underline{\underline{K}}^{(1)} = \int_{V^{(1)}} \underline{\underline{B}}^{(1)T} \underline{\underline{CB}}^{(1)} dV^{(1)} = \int_{-1}^1 \int_{-2}^2 \underline{\underline{B}}^{(1)T} \underline{\underline{CB}}^{(1)} dx dy$$

$$\underline{\underline{K}}^{(2)} = \int_{V^{(2)}} \underline{\underline{B}}^{(2)T} \beta \underline{\underline{B}}^{(2)} dV^{(2)} = \int_{-2}^2 \int_{-2}^2 \underline{\underline{B}}^{(2)T} \beta \underline{\underline{B}}^{(2)} dx dy$$

$$\underline{\underline{M}} = \underline{\underline{M}}^{(1)} + \underline{\underline{M}}^{(2)} ; \quad \underline{\underline{K}} = \underline{\underline{K}}^{(1)} + \underline{\underline{K}}^{(2)} .$$

Problem 2 (10 points):

(a) “Remove Clamps” to eliminate u_1 and u_3 prior to the use of the central difference method.

$$\begin{bmatrix} 0 & 0 & 0 \\ 0 & 2 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \ddot{U}_1 \\ \ddot{U}_2 \\ \ddot{U}_3 \end{bmatrix} + \begin{bmatrix} 2 & -1 & 0 \\ -1 & 4 & -1 \\ 0 & -1 & 2 \end{bmatrix} \begin{bmatrix} U_1 \\ U_2 \\ U_3 \end{bmatrix} = \begin{bmatrix} 0 \\ R_2(t) \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} 0 & 0 & 0 \\ 0 & 2 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \ddot{U}_1 \\ \ddot{U}_2 \\ \ddot{U}_3 \end{bmatrix} + \begin{bmatrix} 2 & -1 & 0 \\ 0 & 3.5 & -1 \\ 0 & -1 & 2 \end{bmatrix} \begin{bmatrix} U_1 \\ U_2 \\ U_3 \end{bmatrix} = \begin{bmatrix} 0 \\ R_2(t) \\ 0 \end{bmatrix}$$

$$\begin{bmatrix} 0 & 0 & 0 \\ 0 & 2 & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} \ddot{U}_1 \\ \ddot{U}_2 \\ \ddot{U}_3 \end{bmatrix} + \begin{bmatrix} 2 & -1 & 0 \\ 0 & 3 & 0 \\ 0 & -1 & 2 \end{bmatrix} \begin{bmatrix} U_1 \\ U_2 \\ U_3 \end{bmatrix} = \begin{bmatrix} 0 \\ R_2(t) \\ 0 \end{bmatrix}$$

$$2\ddot{U}_2 + 3U_2 = R_2(t)$$

Using the central difference method,

$$2' \ddot{U}_2 + 3' U_2 = ' R_2 \quad (1)$$

$${}^t\ddot{U}_2 = \frac{1}{\Delta t^2} ({}^{t+\Delta t}U_2 - 2{}^tU_2 + {}^{t-\Delta t}U_2) \quad (2)$$

$${}^t\dot{U}_2 = \frac{1}{2\Delta t} ({}^{t+\Delta t}U_2 - {}^{t-\Delta t}U_2) \quad (3)$$

Substitute (2) into (1)

$$\frac{2}{\Delta t^2} {}^{t+\Delta t}U_2 = {}^tR_2 - (3 - \frac{4}{\Delta t^2}) {}^tU_2 - \frac{2}{\Delta t^2} {}^{t-\Delta t}U_2$$

To start the solution, we use $2\ddot{U}_2 + 3U_2 = R_2(t)$ at time $t=0$.

Hence, ${}^0\ddot{U}_2 = 0$ since U_2 and R_2 are zero at $t=0$.

We can obtain ${}^{-\Delta t}U_2 = 0$ using Eq. (2) and Eq. (3).

$$0 = {}^0\ddot{U}_2 = \frac{1}{\Delta t^2} ({}^{\Delta t}U_2 - 2{}^0U_2 + {}^{-\Delta t}U_2)$$

$$0 = {}^0\dot{U}_2 = \frac{1}{2\Delta t} ({}^{\Delta t}U_2 - {}^{-\Delta t}U_2)$$

Determine ${}^{t+\Delta t}U_1$ and ${}^{t+\Delta t}U_3$ by $\begin{bmatrix} {}^{t+\Delta t}U_1 \\ {}^{t+\Delta t}U_3 \end{bmatrix} = \begin{bmatrix} \frac{1}{2} \\ \frac{1}{2} \end{bmatrix} {}^{t+\Delta t}U_2$.

$$(b) \Delta t_{cr} = \frac{2}{\omega} = 2\sqrt{\frac{2}{3}} = 1.633$$

For stability, Δt should be smaller than Δt_{cr} . The frequency content of the load can be roughly approximated by $\hat{\omega} = \frac{2\pi}{80}$ where $\hat{T} = 80$ so that $\frac{\hat{\omega}}{\omega} = 0.0641$. Because this value is quite close to zero, we can assume the response to be almost static. Therefore, $\Delta t = 1.6$ is a well selected time step for the stability and the accuracy.

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