MIT OPENCOURSEWARE
MASSACHUSETTS INSTITUTE OF TECHNOLOGY

6.776
High Speed Communication Circuits
Lecture 3
Wave Guides and Transmission Lines

Massachusetts Institute of Technology

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Maxwell's Equations

- **General form:**

$$\nabla \times E = -\mu \frac{dH}{dt} \qquad (1)$$

$$\nabla \times H = J + \epsilon \frac{dE}{dt} \qquad (2)$$

$$\nabla \cdot \epsilon E = \rho \qquad (3)$$

$$\nabla \cdot \mu H = 0 \qquad (4)$$

- **Assumptions for free space and transmission line propagation**
  - **No charge buildup:** $\rho = 0$
  - **No free current:** $J = 0$

Maxwell's Equations in Free Space

Take Curl of (1):

$$\nabla \times \nabla \times E = -\nabla \times \left(\mu \frac{\partial H}{\partial t} \right) = -\mu \frac{\partial}{\partial t} \left(\nabla \times H \right) \qquad (5)$$

From (2)

$$\mu \frac{\partial}{\partial t} \left(\nabla \times H \right) = \mu \varepsilon \frac{\partial^2 E}{\partial t^2} \qquad (6)$$

Vector identity + (3)

$$\nabla \times \nabla \times E = \nabla \left(\nabla \cdot E \right) - \nabla^2 E = -\nabla^2 E \qquad (7)$$

Simplified Maxwell's Equations

Putting together (5), (6) and (7):

$$\nabla^2 E + \mu\varepsilon \frac{\partial^2 E}{\partial t^2} = 0 \qquad (8)$$

Similarly for H

$$\nabla^2 H + \mu\varepsilon \frac{\partial^2 H}{\partial t^2} = 0 \qquad (9)$$

For simplicity, assume only z-direction

$$\nabla^2 E = \frac{\partial^2 E}{\partial z^2} \quad \text{and} \quad \nabla^2 H = \frac{\partial^2 H}{\partial z^2} \qquad (10)$$

Solutions to Maxwell's Equations

(10) reduces to

$$\frac{\partial^2 E}{\partial z^2} + \mu\varepsilon \frac{\partial^2 E}{\partial t^2} = 0 \qquad (11)$$

Similarly for H

$$\frac{\partial^2 H}{\partial z^2} + \mu\varepsilon \frac{\partial^2 H}{\partial t^2} = 0 \qquad (12)$$

(11) and (12) can be satisfied by any function in the form

$f\left(z \pm vt\right)$ **where** $v = \dfrac{1}{\sqrt{\mu\varepsilon}}$

Calculating Propagation Speed

- The function f is a function of time AND position

- Velocity calculation

$$z \pm vt = \text{constant}$$

$$\frac{\partial z}{\partial t} = \pm v$$

- The solution propagates in the z or –z direction with a

velocity of $v = \frac{1}{\sqrt{\mu\varepsilon}}$

Assume Sinusoidal Steady-State

E and H solutions are in the form

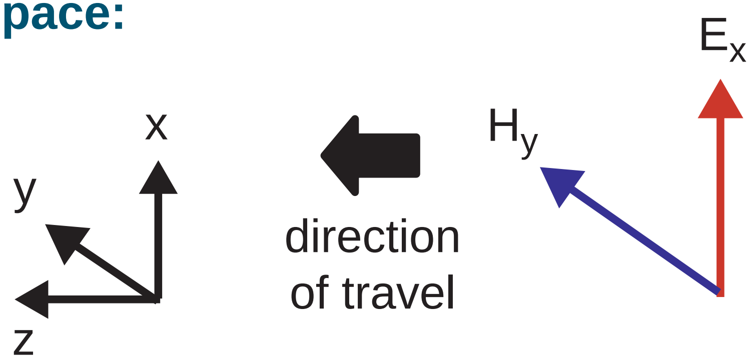
$$Ae^{j\omega(t \pm \frac{z}{v})} = Ae^{j(\omega t \pm kz)}$$

Where

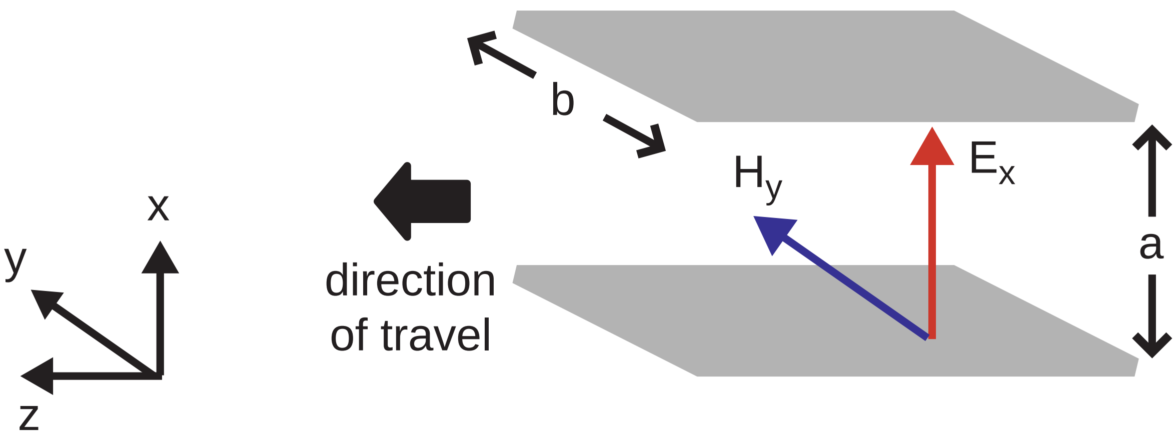
$$k = \frac{\omega}{v} = \omega\sqrt{\mu\varepsilon}$$

Assumptions

- **Orientation and direction**
  - **E field is in x-direction and traveling in z-direction**
  - **H field is in y-direction and traveling in z-direction**
  - **In freespace:**



- **For transmission line (TEM mode)**



Solutions

- **Fields change only in time and in z-direction**

$$E = \hat{x} E_x(z,t) = \hat{x} E_o e^{-jkz} e^{jwt}$$

$$H = \hat{y} H_y(z,t) = \hat{y} H_o e^{-jkz} e^{jwt}$$

- **Implications:**

$$\frac{dE_x(z,t)}{dz} = -jkE_x(z,t), \quad \frac{dE_x(z,t)}{dt} = jwE_x(z,t)$$

$$\frac{dH_y(z,t)}{dz} = -jkH_y(z,t), \quad \frac{dH_y(z,t)}{dt} = jwH_y(z,t)$$

Evaluate Curl Operations in Maxwell's Formula

- **Definition**

$$\nabla \times E = \hat{x}\left(\frac{dE_z}{dy} - \frac{dE_y}{dz}\right) + \hat{y}\left(\frac{dE_x}{dz} - \frac{dE_z}{dx}\right) + \hat{z}\left(\frac{dE_y}{dx} - \frac{dE_x}{dy}\right)$$

$$\nabla \times H = \hat{x}\left(\frac{dH_z}{dy} - \frac{dH_y}{dz}\right) + \hat{y}\left(\frac{dH_x}{dz} - \frac{dH_z}{dx}\right) + \hat{z}\left(\frac{dH_y}{dx} - \frac{dH_x}{dy}\right)$$

Evaluate Curl Operations in Maxwell's Formula

- **Definition**

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$$\nabla\times H = \hat{x}\left(\frac{dH_z}{dy}-\frac{dH_y}{dz}\right)+\hat{y}\left(\frac{dH_x}{dz}-\frac{dH_z}{dx}\right)+\hat{z}\left(\frac{dH_y}{dx}-\frac{dH_x}{dy}\right)$$

- **Given the previous assumptions**

$$\nabla\times E = \hat{y}\,\frac{dE_x(z,t)}{dz} = -\hat{y}\;jkE_x(z,t)$$

$$\nabla\times H = -\hat{x}\,\frac{dH_y(z,t)}{dz} = \hat{x}\;jkH_y(z,t)$$

Now Put All the Pieces Together

- **Solve Maxwell's Equation (1)**

$$\nabla \times E = -\mu \frac{dH}{dt} \Rightarrow -\hat{y}\; jkE_x(z,t) = -\hat{y}\; \mu jwH_y(z,t)$$

$$\Rightarrow \frac{E_x(z,t)}{H_y(z,t)} = \frac{\mu w}{k} \quad \text{(intrinsic impedance)}$$

Now Put All the Pieces Together

- **Solve Maxwell's Equations (1) and (2)**

$$\nabla \times E = -\mu \frac{dH}{dt} \Rightarrow -\hat{y}\; jkE_x(z,t) = -\hat{y}\; \mu j w H_y(z,t)$$

$$\Rightarrow \frac{E_x(z,t)}{H_y(z,t)} = \frac{\mu w}{k} \quad \text{(intrinsic impedance)}$$

$$\Rightarrow \text{intrinsic impedance} = \frac{\mu w}{k} = \frac{\mu w}{w\sqrt{\mu\epsilon}} = \sqrt{\frac{\mu}{\epsilon}}$$

Freespace Values

- **Constants**

$$\epsilon = \epsilon_o = \frac{1}{36\pi} \times 10^{-9} \text{ F/m}$$

$$\mu = \mu_o = 4\pi \times 10^{-7} \text{ H/m}$$

- **Impedance**

$$\sqrt{\frac{\mu}{\epsilon}} = \sqrt{\frac{\mu_o}{\epsilon_o}} = \text{ 377 Ohms}$$

- **Propagation speed**

$$\frac{1}{\sqrt{\mu\epsilon}} = \frac{1}{\sqrt{\mu_o\epsilon_o}} = 30 \times 10^9 \text{ cm/s}$$

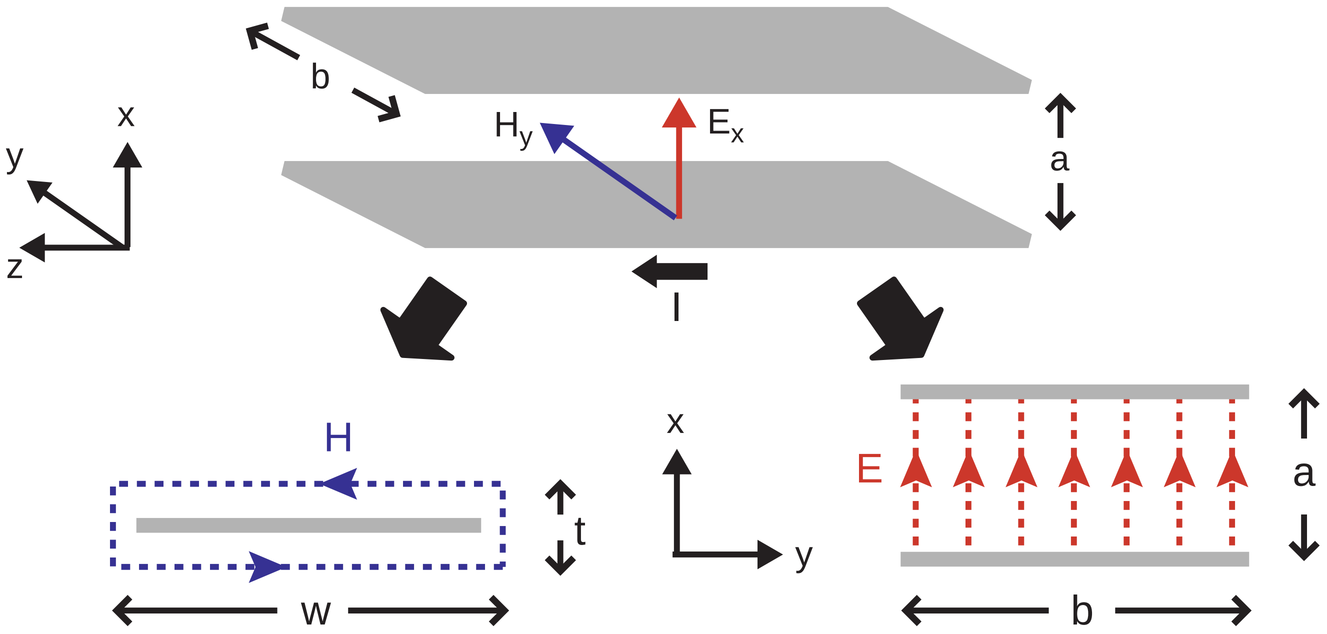
- **Wavelength of 30 GHz signal**

$$\lambda = \frac{T}{\sqrt{\mu\epsilon}} = \frac{1}{f\sqrt{\mu_o\epsilon_o}} = \text{ 1 cm}$$

Voltage and Current

- **Definitions:** $V = \int_{C_t} E \cdot dl$ (path integral)

  $I = \oint_{C_o} H \cdot dl$ (contour integral)

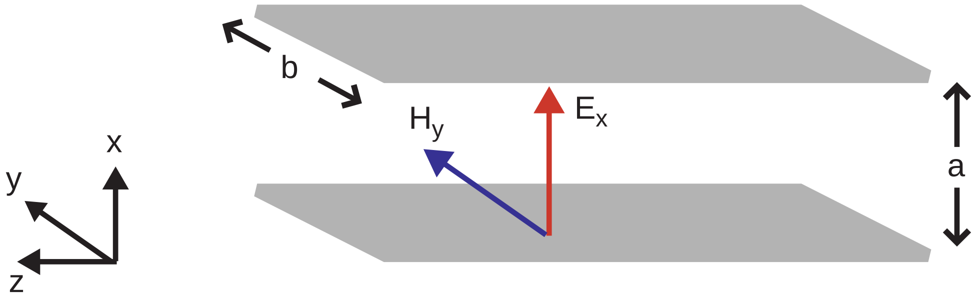


$I = (2w + 2t)H$

$V = aE$

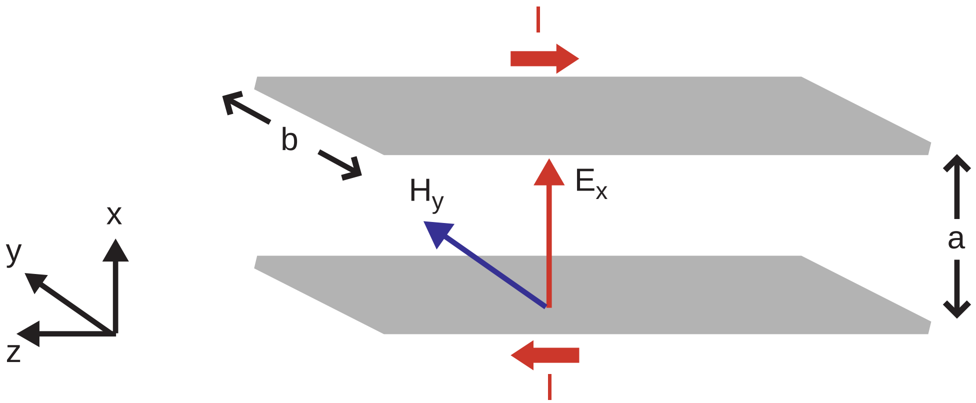
Parallel Plate Waveguide

- **E-field and H-field are influenced by plates**



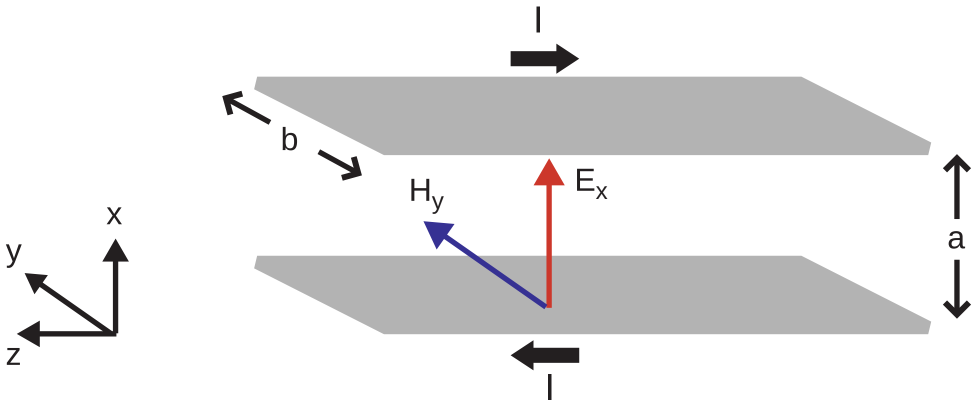
Current and H-Field

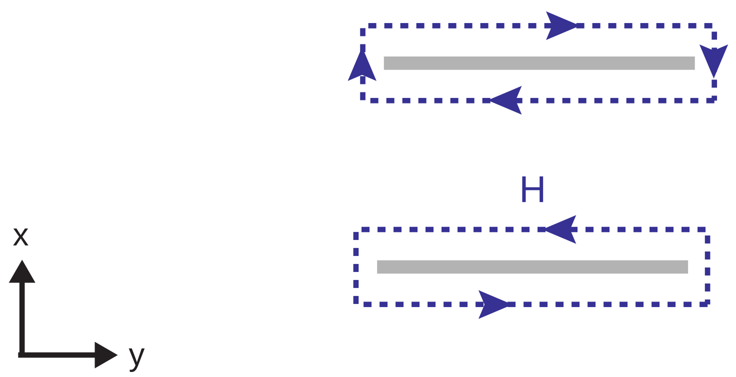
- **Assume that (AC) current is flowing**



Current and H-Field

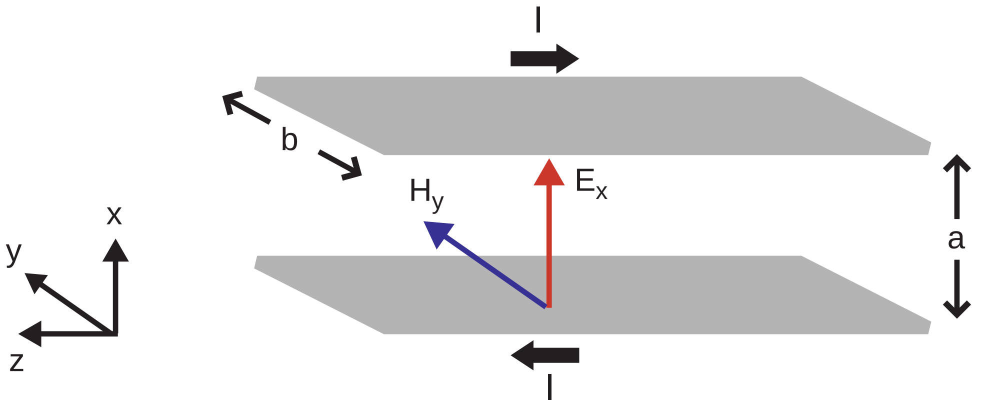
- **Current flowing down waveguide influences H-field**

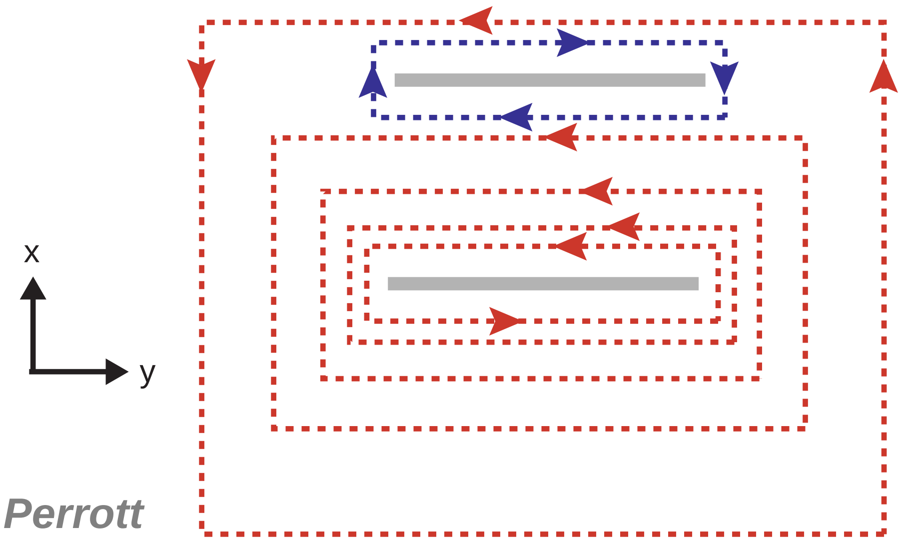




Current and H-Field

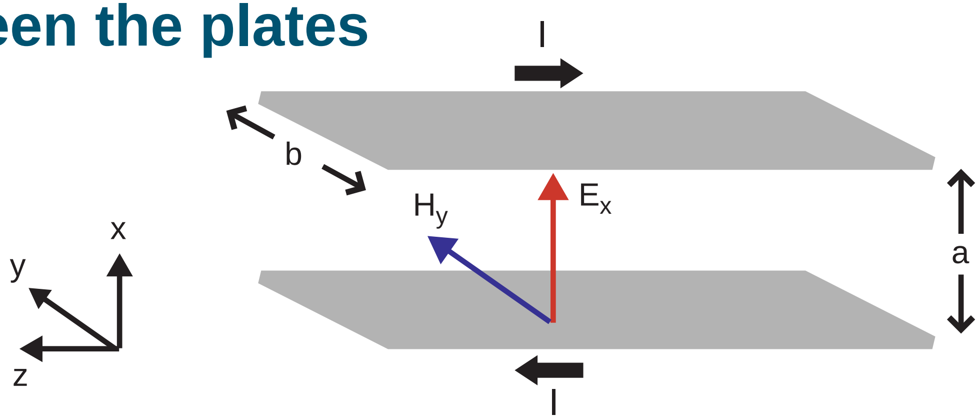
- **Flux from one plate interacts with flux from the other plate**

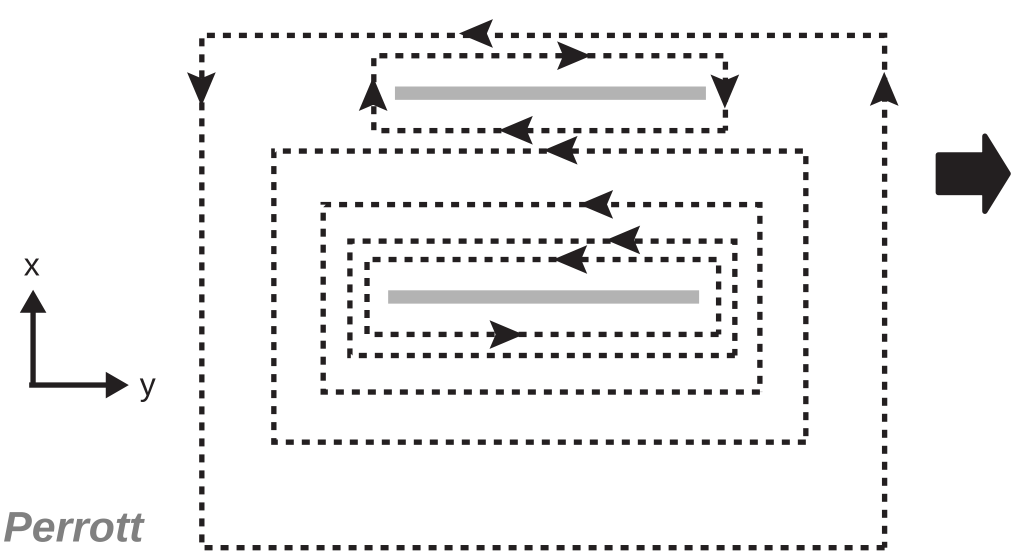


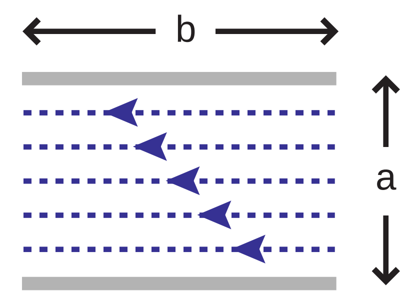


Current and H-Field

- **Approximate H-Field to be uniform and restricted to lie between the plates**



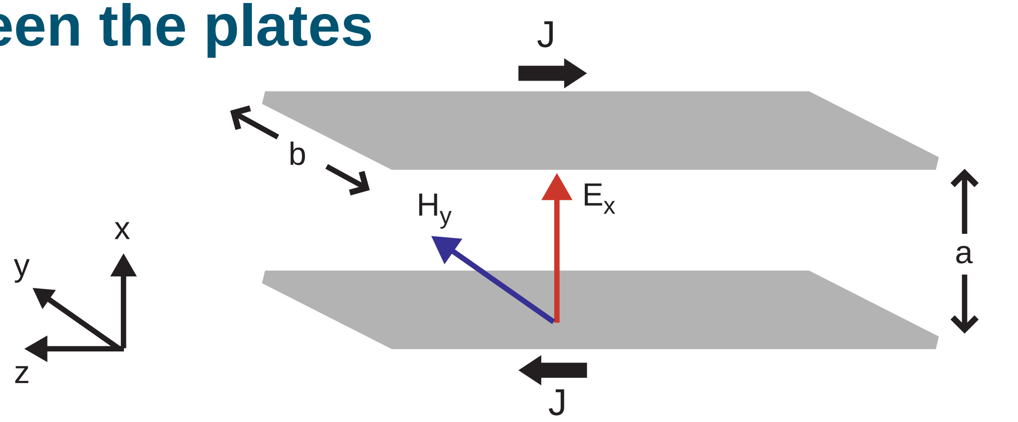


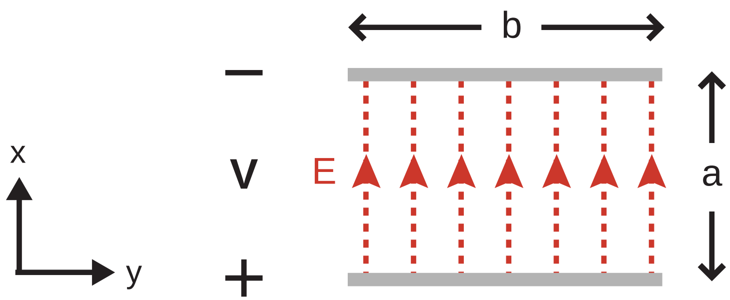


$$I = bH$$

Voltage and E-Field

- **Approximate E-field to be uniform and restricted to lie between the plates**





$$V = aE$$

Back to Maxwell's Equations

- **From previous analysis**

$$\nabla \times E = -\mu \frac{dH}{dt} \Rightarrow jkE_x(z,t) = jw\mu H_y(z,t)$$

$$\nabla \times H = \epsilon \frac{dE}{dt} \Rightarrow jkH_y(z,t) = jw\epsilon E_x(z,t)$$

- **These can be equivalently written as**

$$jk\left(aE_x(z,t)\right) = jw\mu \frac{a}{b}\left(bH_y(z,t)\right) \Rightarrow \boxed{jkV(z,t) = jwLI(z,t)}$$

$$jk(bH_y(z,t)) = jw\epsilon \frac{b}{a}(aE_x(z,t)) \Rightarrow \boxed{jkI(z,t) = jwCV(z,t)}$$

- **Where**

$$L = \mu \frac{a}{b} \quad \text{(inductance per unit length - H/m)}$$

$$C = \epsilon \frac{b}{a} \quad \text{(capacitance per unit length - F/m)}$$

Wave Equation for Transmission Line (TEM)

- **Key formulas**

$$jkV(z,t) = jwLI(z,t) \qquad (1)$$

$$jkI(z,t) = jwCV(z,t) \qquad (2)$$

- **Substitute (2) into (1)**

$$jkV(z,t) = jwL\left(\frac{w}{k}CV(z,t)\right) \Rightarrow (k^2 - w^2LC)V(z,t) = 0$$

$$\boxed{\Rightarrow\ k = w\sqrt{LC}}$$

- **Characteristic impedance (use Equation (1))**

$$\frac{V(z,t)}{I(z,t)} = \frac{wL}{k} = \frac{wL}{w\sqrt{LC}} = \boxed{\sqrt{\frac{L}{C}}}$$

Connecting to the Real World

- **Typical of sinusoidal analysis usingphasors, the solutions are complex**

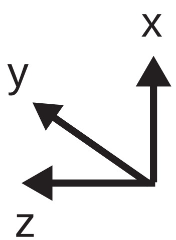
$$V(z,t) = V_o e^{-jkz} e^{jwt} = V_o e^{-j(wt-kz)}$$

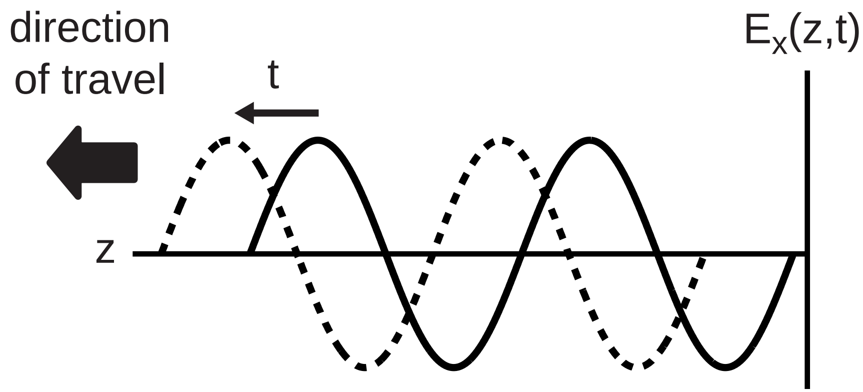
- **Take the real part of the solution to find the real-world solution:**

$$v(z,t) = Re(V(z,t)) = V_o cos(wt - kz)$$

Calculating Propagation Speed

- **The resulting cosine wave is a function of time AND position**





$$v(z,t) = V_o \cos(wt - kz)$$

- **Consider "riding" one part of the wave**

$$-kz + wt = \text{constant}$$

- **Velocity calculation**

$$\frac{dz}{dt} = \frac{d}{dt}\left(\frac{wt}{k}\right) = \frac{w}{k} = \frac{w}{w\sqrt{LC}} = \boxed{\frac{1}{\sqrt{LC}}}$$

Integrated Circuit Values

- **Constants**

$$\epsilon = \epsilon_r \epsilon_o \quad (\epsilon_r = 3.9, 11.7, 4.4 \text{ in } SiO_2,\ Si,\ \text{FR4, respectively})$$

$$\mu = \mu_r \mu_o \quad (\mu_r = 1 \text{ for the above materials})$$

- **Impedance (geometry/material dependant)**

$$\sqrt{\frac{L}{C}} = \sqrt{\frac{\mu(a/b)}{\epsilon(b/a)}} = \sqrt{\frac{\mu}{\epsilon}}\left(\frac{a}{b}\right)$$

Integrated Circuit Values

- **Constants**

$\epsilon = \epsilon_r \epsilon_o \quad (\epsilon_r = 3.9, 11.7, 4.4 \text{ in } SiO_2,\ Si,\ \text{FR4, respectively})$

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- **Impedance (geometry/material dependant)**

$$\sqrt{\frac{L}{C}} = \sqrt{\frac{\mu(a/b)}{\epsilon(b/a)}} = \sqrt{\frac{\mu}{\epsilon}}\left(\frac{a}{b}\right)$$

- **Propagation speed (geometry independent, material dependent)**

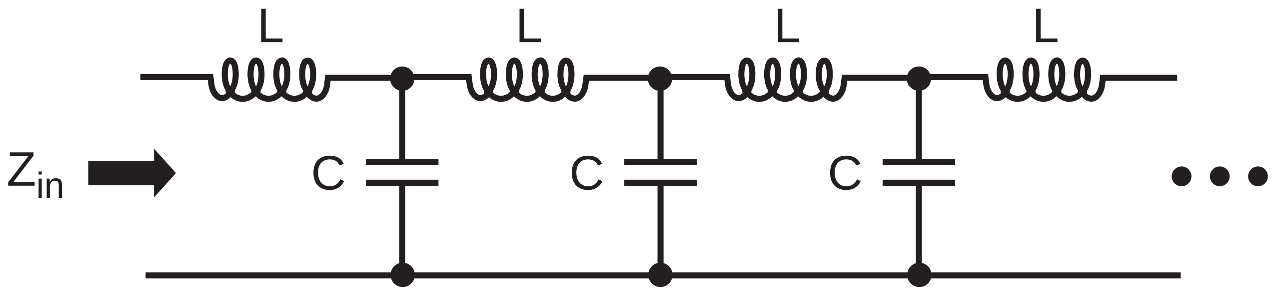
$$\frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{\mu(a/b)\epsilon(b/a)}} = \frac{1}{\sqrt{\mu\epsilon}} = \frac{30 \times 10^9}{\sqrt{\mu_r \epsilon_r}} \text{ cm/s}$$

- **Wavelength of 30 GHz signal in silicon dioxide**

$$\lambda = \frac{T}{\sqrt{\mu\epsilon}} = \frac{1}{f\sqrt{3.9\mu_o\epsilon_o}} = 1/2 \text{ cm}$$

LC Network Analogy of Transmission Line (TEM)

- **LC network analogy**



- **Calculate input impedance**

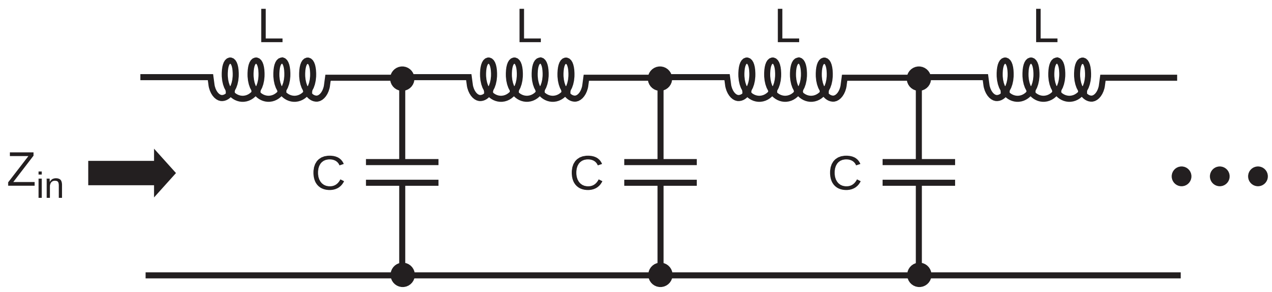
$$Z_{in} = sL + (1/sC)||Z_{in} = sL + \frac{Z_{in}}{1 + Z_{in}sC}$$

$$\Rightarrow \quad Z_{in}^2 - sLZ_{in} - L/C = 0$$

$$\Rightarrow \quad Z_{in} = \frac{sL}{2}\left(1 \pm \sqrt{1 + \frac{4}{s^2LC}}\right)$$

LC Network Analogy of Transmission Line (TEM)

- **LC network analogy**



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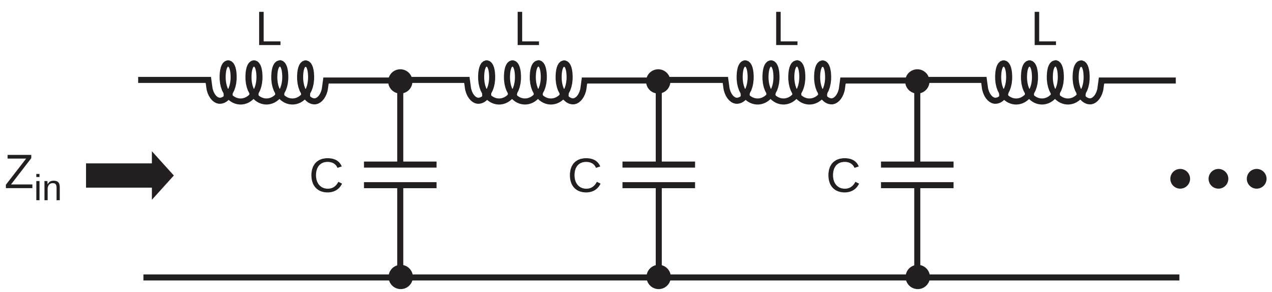
$$\Rightarrow \quad Z_{in}^2 - sLZ_{in} - L/C = 0$$

$$\Rightarrow \quad Z_{in} = \frac{sL}{2}\left(1 \pm \sqrt{1 + \frac{4}{s^2LC}}\right)$$

$$\text{for } |s| \ll \frac{1}{\sqrt{LC}} \quad \Rightarrow \quad Z_{in} \approx \frac{sL}{2}\left(1 \pm \frac{2}{s\sqrt{LC}}\right) \approx \sqrt{\frac{L}{C}}$$

How are Lumped LC and Transmission Lines Different?

- **In transmission line, L and C values are infinitely small**
  - **It is always true that** $|s| \ll \dfrac{1}{\sqrt{LC}}$

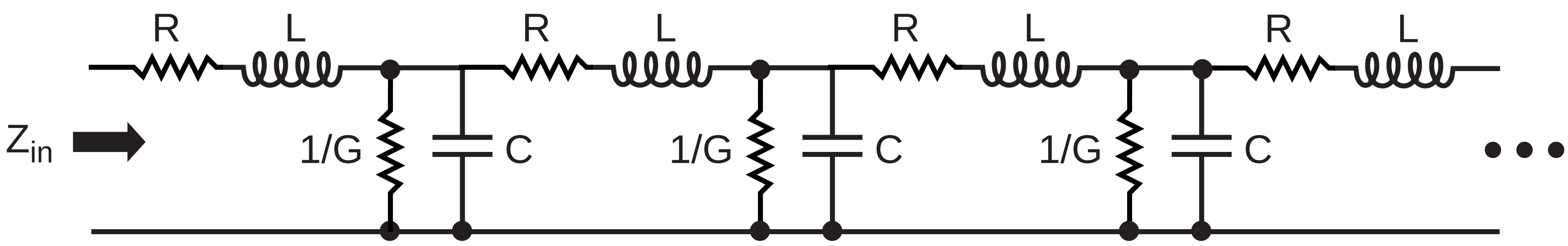


- **For lumped LC, L and C have finite values**
  - **Finite frequency range for** $|s| \ll \dfrac{1}{\sqrt{LC}}$

$$Z_{in} = \frac{sL}{2}\left(1 \pm \sqrt{1 + \frac{4}{s^2LC}}\right) \Rightarrow \text{want } |s| < \frac{2}{\sqrt{LC}} \text{ for real } Z_{in}$$

Lossy Transmission Lines

- **Practical transmission lines have losses in their conductor and dielectric material**
  - **We model such loss by including resistors in the LC model**



- **The presence of such losses has two effects on signals traveling through the line**
  - **Attenuation**
  - **Dispersion (i.e., bandwidth degradation)**
- **See textbook for analysis**