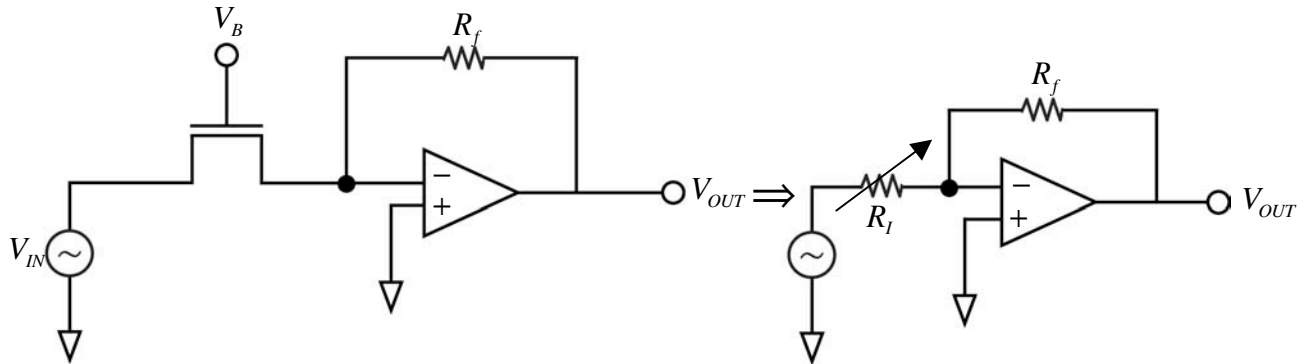


6.301 Solid State Circuits

Recitation 8: LM172 AGC AM IF Strip

Prof. Joel L. Dawson

The LM172 AGC AM IF strip gives us a rather rich set of circuit tricks to add to our toolbox. One useful function to be able to realize in analog systems is a variable gain, where the gain is varied by an analog signal. For example, take the following op-amp circuit:



In the small-signal view of the world, the MOSFET looks like a variable resistor (if we bias things right). So the transfer function becomes

$$\frac{V_{OUT}}{V_{IN}} = -\frac{R_f}{R_I(V_B)}$$

Because R_I is a function of V_B .

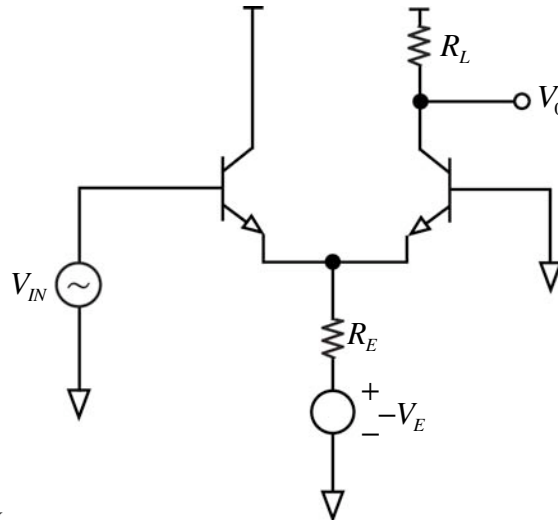
For our class exercise, let's explore a bipolar-friendly expression of this concept.

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CLASS EXERCISE: Consider the emitter-coupled pair:



Remembering that $g_m = \frac{qI_C}{kT}$, derive the gain of this amplifier as a function of V_E .

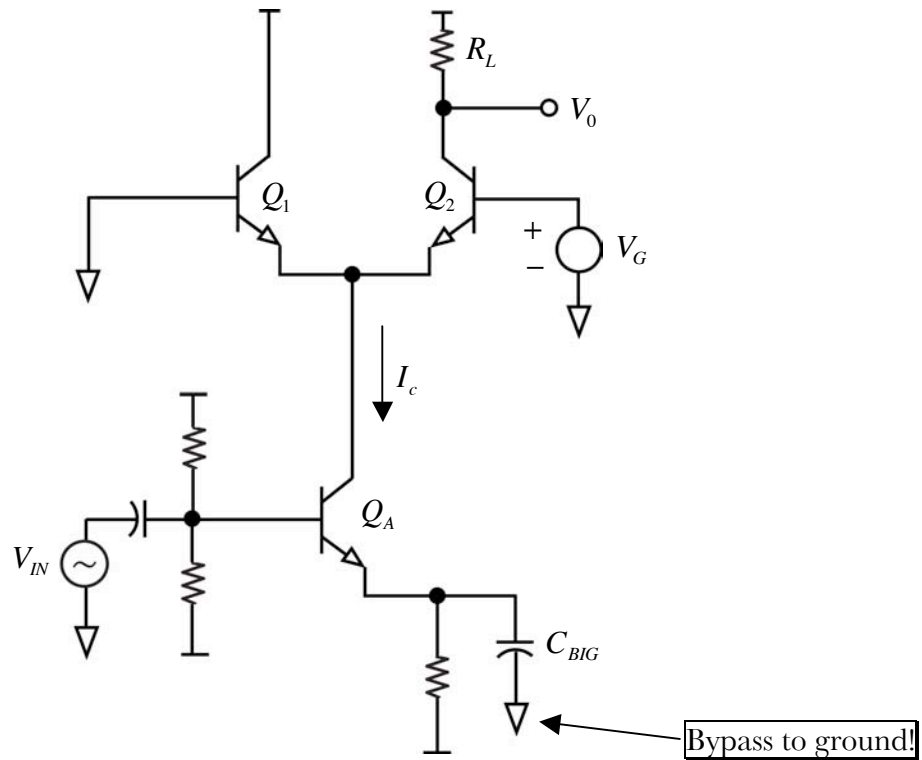
(Workspace)

There are other ways to implement this variable gain idea. In lecture yesterday, Prof. Roberge spoke of “current stealing” as a way of varying the gain. We can examine that concept here in a simpler context:

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When $V_G = 0$, the output current from Q_A gets split evenly between Q_1 and Q_2the gain is therefore $\frac{1}{2} g_{mA} R_L$, as half of the output signal current is “stolen” by Q_1 . Looking in Gray and Meyer, we can find the function of I_C that actually winds up going through R_L as

$$\frac{I_{C2}}{I_C} = \frac{\frac{\beta_2}{1 + \beta_2}}{1 + \exp\left(-\frac{V_G}{V_T}\right)} = \frac{\alpha_2}{1 + \exp\left(-\frac{V_G}{V_T}\right)}$$

The gain for this circuit is thus

$$a_v = \left(\frac{\alpha_2}{1 + \exp\left(-\frac{V_G}{V_T}\right)} \right) g_m R_L$$

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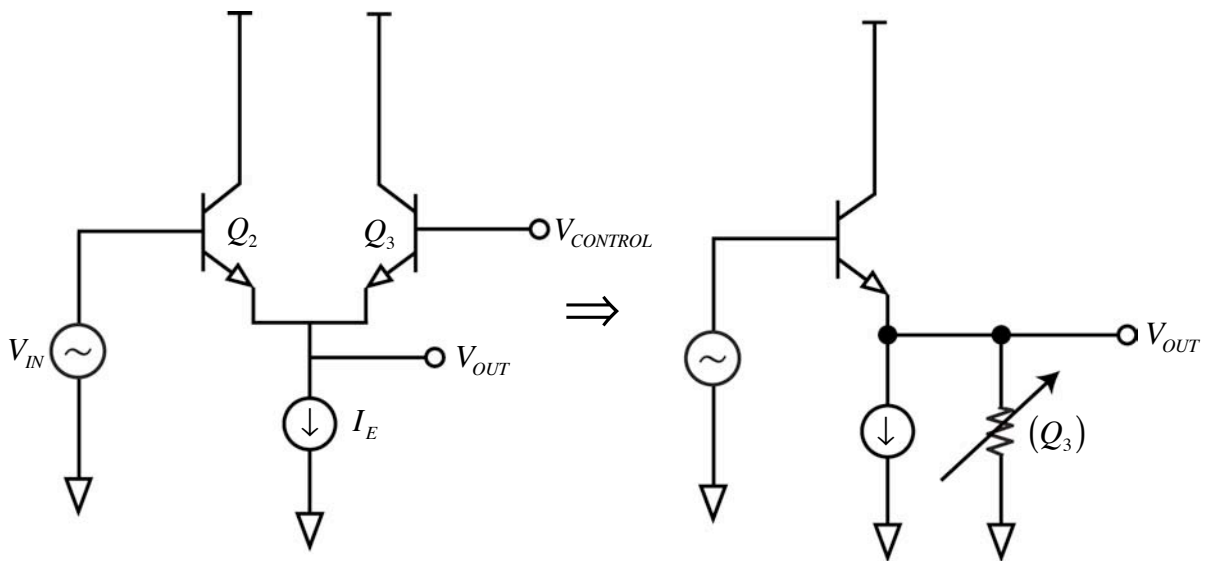
Prof. Joel L. Dawson

which for

$$V_G \gg \frac{kT}{q} (= V_T) \rightarrow a_v \approx g_m R_L$$

$$V_G \ll -\frac{kT}{q} \rightarrow a_v \approx 0$$

The LM172 has yet another approach to solving this problem. Look at Q_2 and Q_3 , and see an emitter follower (Q_2) with a dynamic load (impedance looking into the emitter of Q_3).



Now, again consulting Gray and Meyer,

$$I_{C3} = \frac{\alpha_F I_E}{1 + \exp\left(-\frac{V_{CONTROL}}{V_T}\right)}, \quad I_{C2} = \frac{\alpha_F I_E}{1 + \exp\left(\frac{V_{CONTROL}}{V_T}\right)}$$

For an emitter follower with resistance R_E in the emitter, the voltage gain is

$$a_v = \frac{(\beta + 1)R_E}{r_{\pi 2} + (\beta + 1)R_E}$$

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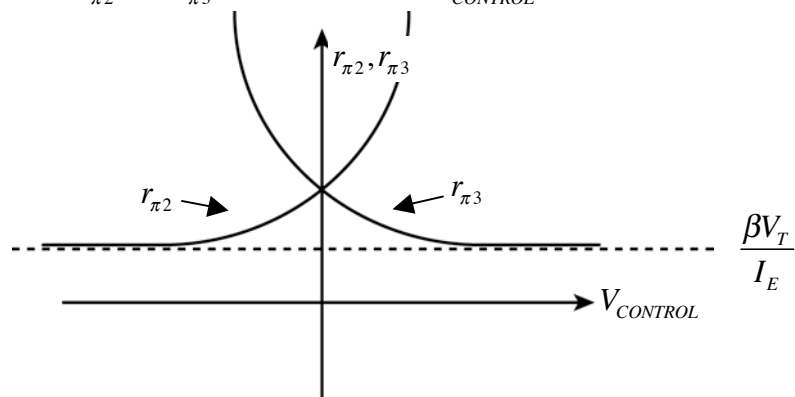
But here, $R_E = \frac{r_{\pi 3}}{\beta + 1}$. Assuming all β s are equal,

$$a_v = \frac{r_{\pi 3}}{r_{\pi 2} + r_{\pi 3}}$$

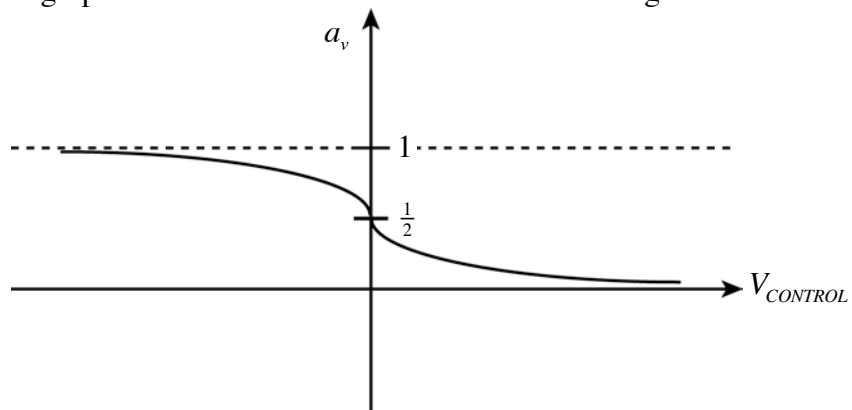
Recalling that r_{π} is inversely proportional to I_C

$$r_{\pi} = \beta \frac{V_T}{I_C}$$

We can qualitatively sketch $r_{\pi 2}$ and $r_{\pi 3}$ as a function of $V_{CONTROL}$:



The corresponding gain graph for this circuit would then look something like



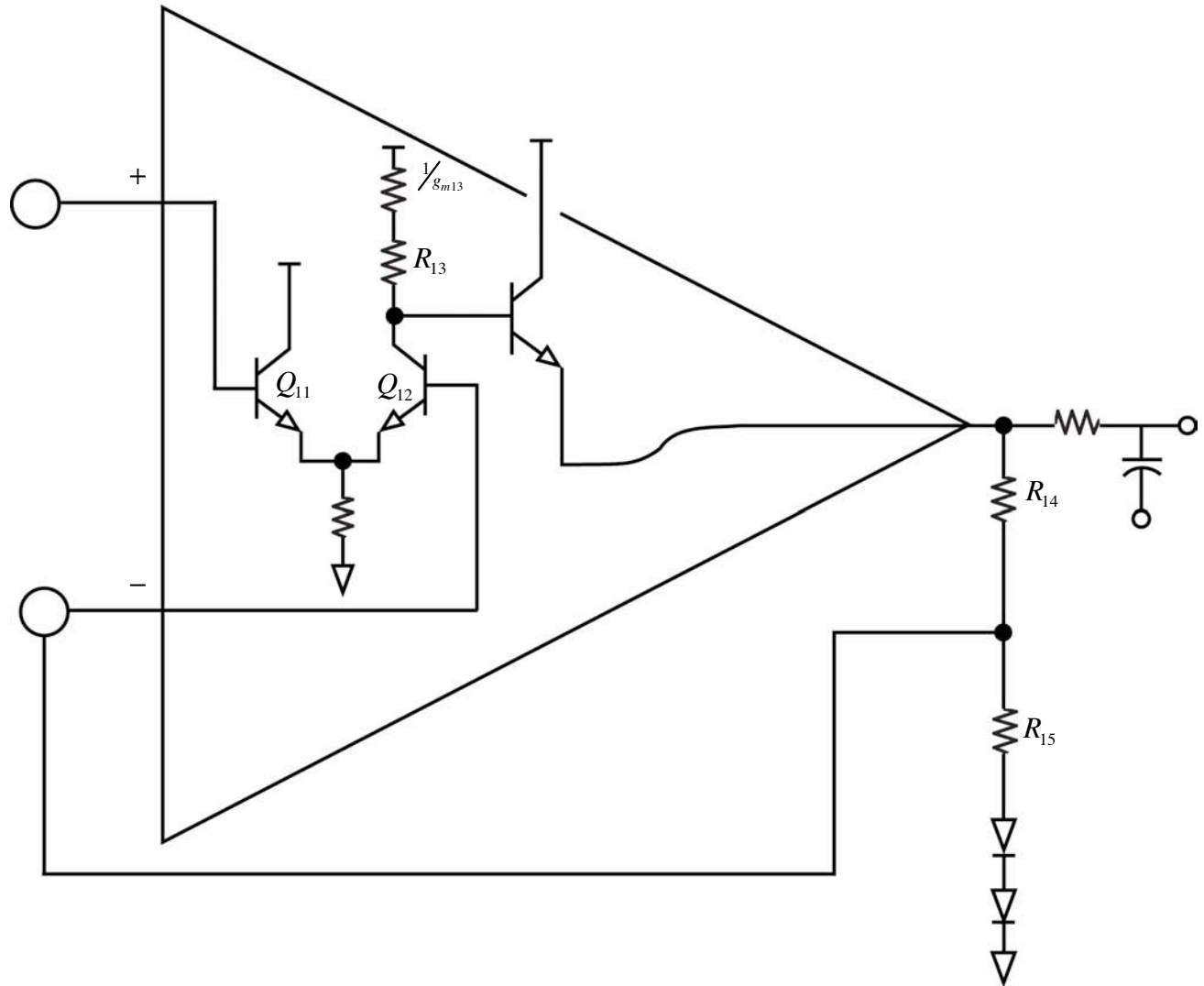
There's also an op-amp hidden in this chip. Can you find it?

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Look at Q_{11} , Q_{12} , and Q_{14}



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