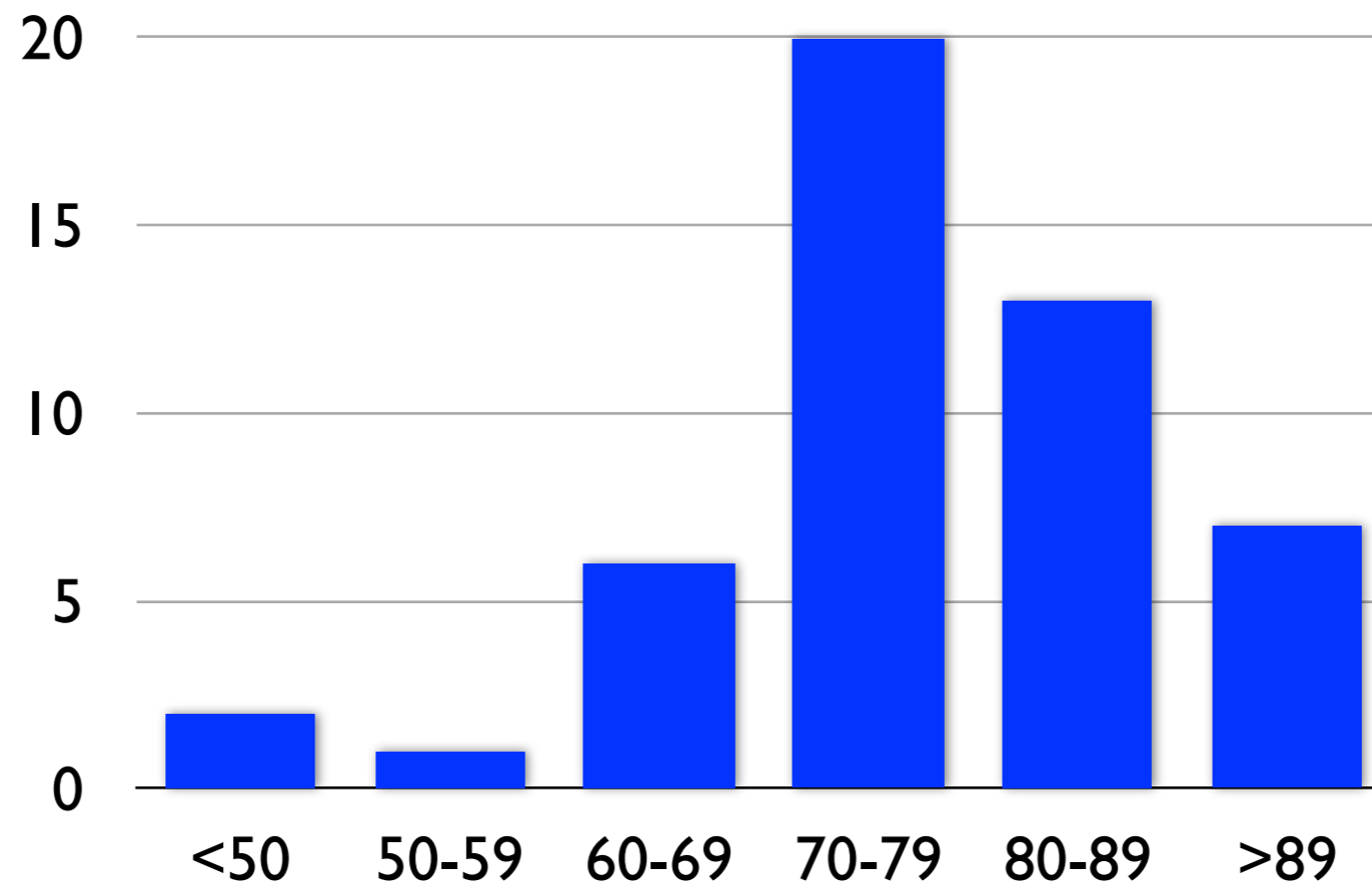


# 10.34: Numerical Methods Applied to Chemical Engineering

Lecture 18:  
Differential Algebraic Equations

# Quiz I Results

- Mean: 77
- Standard deviation: 12



# Recap

- Numerical integration
- Implicit methods for ODE-IVPs

# Recap

- Improper integrals:

- Of the sort: 
$$\int_{t_0}^{\infty} \mathbf{f}(\tau) d\tau$$

- Can be split into two domains of integration

$$\int_{t_0}^{\infty} \mathbf{f}(\tau) d\tau = \int_{t_0}^{t_f} \mathbf{f}(\tau) d\tau + \int_{t_f}^{\infty} \mathbf{f}(\tau) d\tau$$

- The first integral can be handled with ODE-IVP methods or polynomial interpolation

- The second must be handled separately through either:

- transformation onto a finite domain

- or substitution of an asymptotic approximation

- This same idea applies to integrable singularities as well.

# Recap

- Improper integrals:
  - Example:

$$\begin{aligned} & \int_0^{t_f} \frac{\cos \tau}{\sqrt{\tau}} d\tau \\ & \approx \int_0^{t_0} \frac{1 - \tau^2/2}{\sqrt{\tau}} d\tau + \int_{t_0}^{t_f} \frac{\cos \tau}{\sqrt{\tau}} d\tau \\ & \approx 2t_0^{1/2} - \frac{1}{5}t_0^{5/2} + \int_{t_0}^{t_f} \frac{\cos \tau}{\sqrt{\tau}} d\tau \end{aligned}$$

# Recap

- Example:
  - Use implicit Euler to solve:

$$\frac{dx}{dt} = \lambda x, x(0) = x_0$$

Give a closed form formula for the numerical solution

# Recap

- Example:
- Use implicit Euler to solve:

$$\frac{dx}{dt} = \lambda x, x(0) = x_0$$

- Let:  $x_k = x(k\Delta t)$

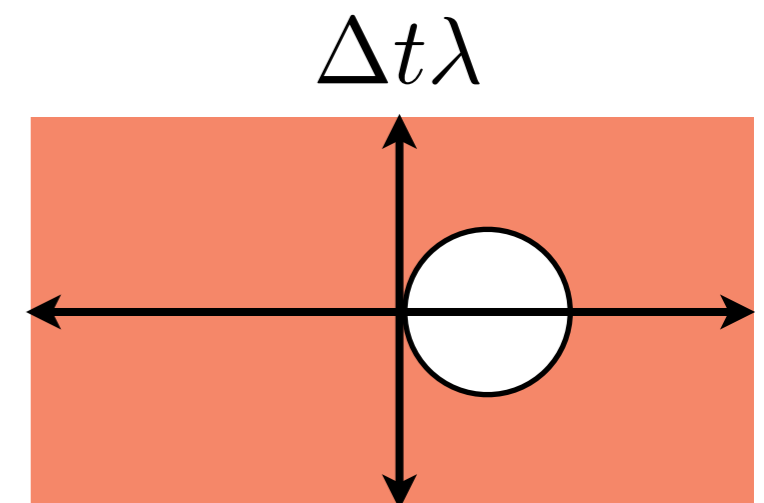
$$x_{k+1} = x_k + \Delta t \lambda x_{k+1}$$

$$x_{k+1} = \frac{1}{1 - \Delta t \lambda} x_k$$

$$x_k = \left( \frac{1}{1 - \Delta t \lambda} \right)^k x_0$$

- Stability:

$$|1 - \Delta t \lambda| \geq 1 \Rightarrow (1 - \Delta t \operatorname{Re} \lambda)^2 + (\Delta t \operatorname{Im} \lambda)^2 \geq 1$$



# Recap

- Example:
  - Use implicit Euler to solve:

$$\frac{dx}{dt} = \lambda x, x(0) = x_0$$

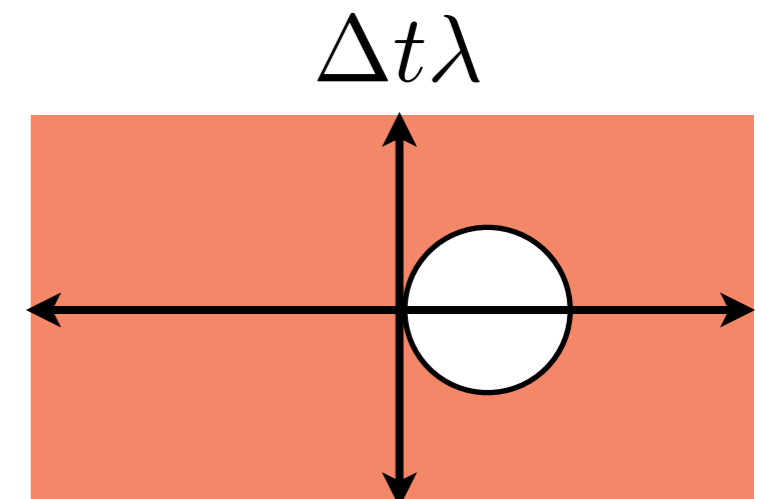
- Numerical solution:

$$x_k = \left( \frac{1}{1 - \Delta t \lambda} \right)^k x_0$$

- Exact solution:

$$x_k = x_0 e^{k\lambda\Delta t}$$

- Stability and accuracy do not correlate!



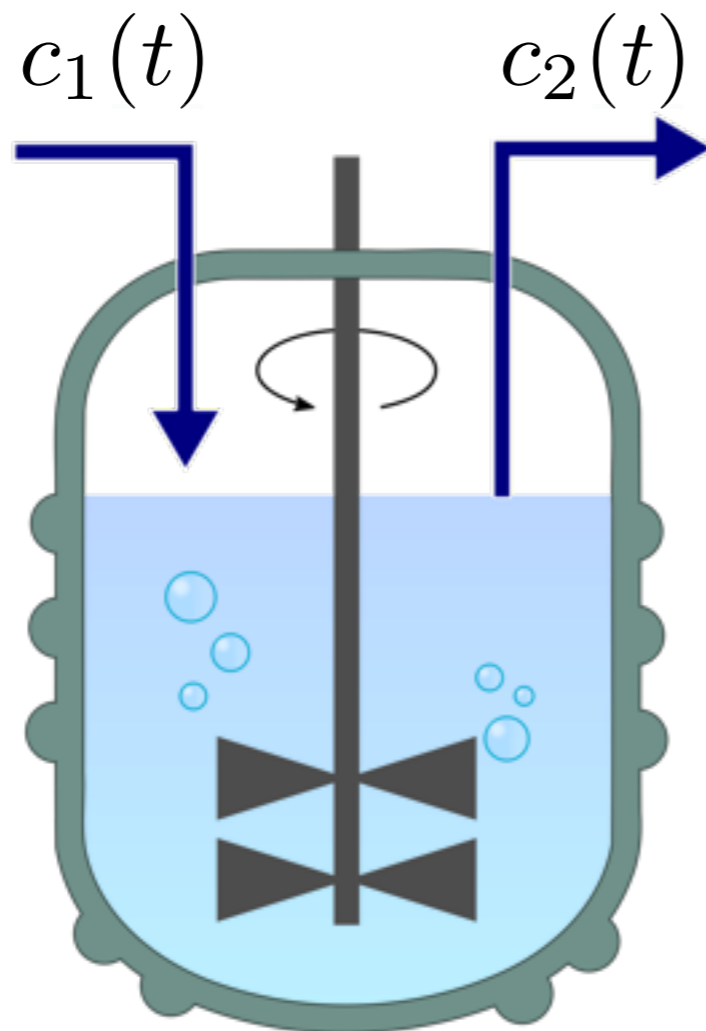


# Differential Algebraic Equations

- Problems of the sort:  $\mathbf{f} \left( \mathbf{x}, \frac{d\mathbf{x}}{dt}, t \right) = 0, \mathbf{x}(0) = \mathbf{x}_0$

- Called “well-posed” when  $\mathbf{x}, \mathbf{f} \in \mathbf{R}^N$

- Example: stirred tank I



$$\frac{dc_2}{dt} = \frac{Q}{V} (c_1(t) - c_2(t))$$

$$c_1(t) = \gamma(t)$$

$$c_1(0) = \gamma(0), c_2(0) = c_0$$

**Solution:**

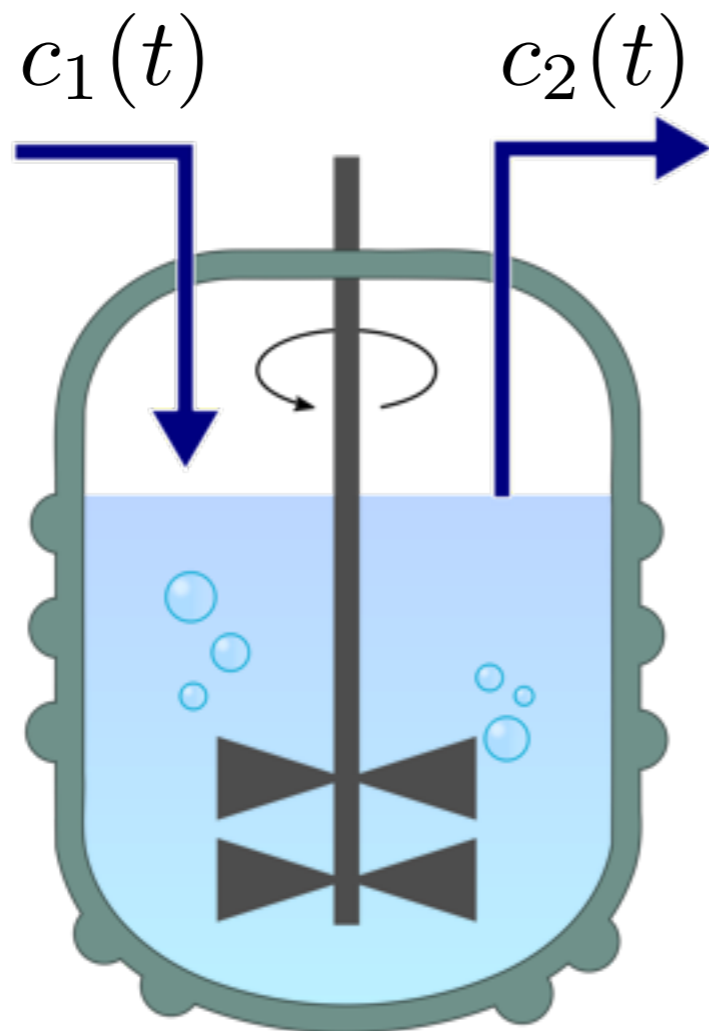
$$c_1(t) = \gamma(t)$$

$$c_2(t) = c_2(0)e^{-(Q/V)t}$$

$$+ \frac{Q}{V} \int_0^t \gamma(t') e^{-(Q/V)(t-t')} dt',$$

# Differential Algebraic Equations

- Problems of the sort:  $\mathbf{f} \left( \mathbf{x}, \frac{d\mathbf{x}}{dt}, t \right) = 0, \mathbf{x}(0) = \mathbf{x}_0$
- Called “well-posed” when  $\mathbf{x}, \mathbf{f} \in \mathbf{R}^N$
- Example: stirred tank I



$$\begin{pmatrix} \frac{dc_2}{dt} - \frac{Q}{V} (c_1(t) - c_2(t)) \\ c_1(t) - \gamma(t) \end{pmatrix} = 0$$

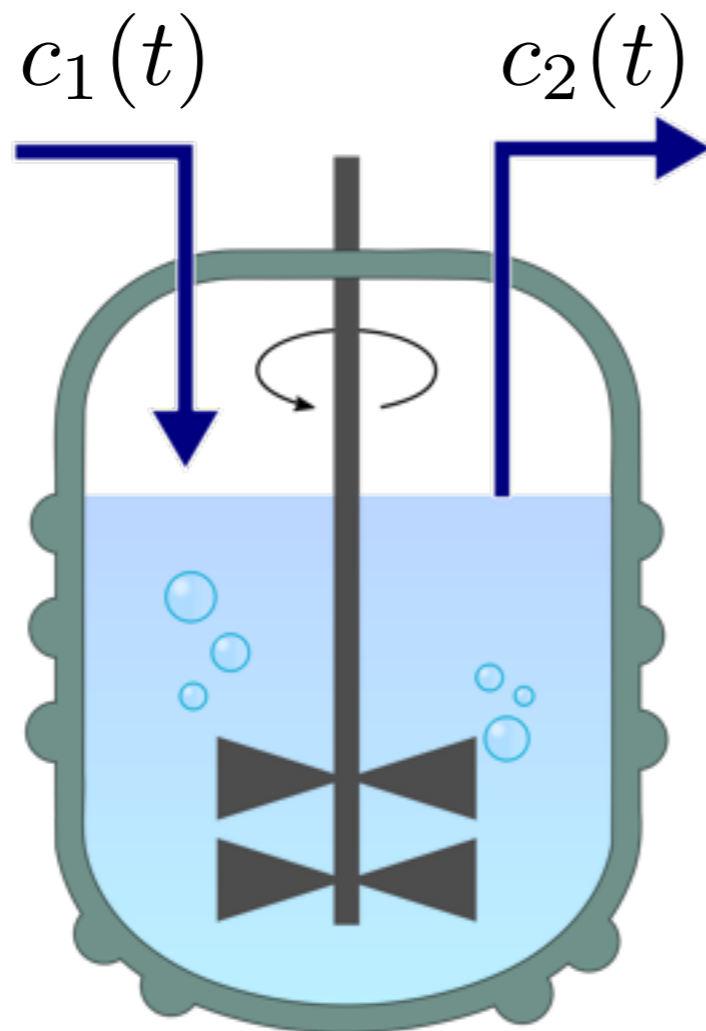
$$\begin{pmatrix} c_1(0) \\ c_2(0) \end{pmatrix} = \begin{pmatrix} \gamma(0) \\ c_0 \end{pmatrix}$$

# Differential Algebraic Equations

- Problems of the sort:  $\mathbf{f} \left( \mathbf{x}, \frac{d\mathbf{x}}{dt}, t \right) = 0, \mathbf{x}(0) = \mathbf{x}_0$

- Called “well-posed” when  $\mathbf{x}, \mathbf{f} \in \mathbf{R}^N$

- Example: stirred tank 2



$$\frac{dc_2}{dt} = \frac{Q}{V} (c_1(t) - c_2(t))$$

$$\underline{c_2(t) = \gamma(t)}$$

$$c_1(t) = c_0, c_2(0) = \gamma(0)$$

Solution:

$$c_1(t) = \gamma(t) + \frac{V}{Q} \dot{\gamma}$$

$$c_2(t) = \gamma(t)$$

# Differential Algebraic Equations

- Common in dynamic simulations involving conservation, constraints, or equilibria.
- Conservation of total:
  - energy
  - mass
  - momentum
  - particle number
  - atomic species
  - charge
- Models of reaction networks utilizing the pseudo-steady-state approximation.
- Models of control neglecting controller dynamics.

# Semi-explicit DAEs

- Problems of the sort:  $\mathbf{M} \frac{d\mathbf{x}}{dt} = \mathbf{f}(\mathbf{x}, t), \mathbf{x}(0) = \mathbf{x}_0$

- $\mathbf{M}$  is called the “mass matrix”

- Stirred tank example I:

$$\begin{pmatrix} \frac{dc_2}{dt} - \frac{Q}{V} (c_1(t) - c_2(t)) \\ c_1(t) - \gamma(t) \end{pmatrix} = 0$$

- Semi-explicit form:

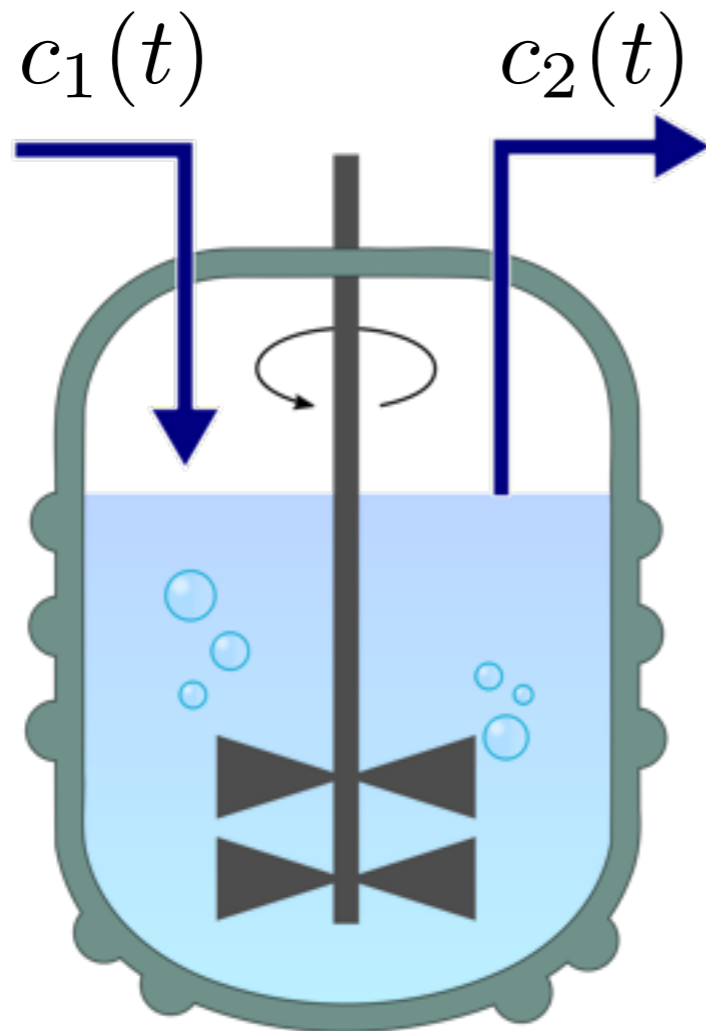
$$\begin{pmatrix} 1 & 0 \\ 0 & 0 \end{pmatrix} \frac{d}{dt} \mathbf{c} = \begin{pmatrix} \frac{Q}{V} & -\frac{Q}{V} \\ -1 & 0 \end{pmatrix} \mathbf{c} + \begin{pmatrix} 0 \\ \gamma(t) \end{pmatrix}$$

- When mass matrix is full rank these problems can be solved by applying typical ODE-IVP techniques to:

$$\frac{d\mathbf{x}}{dt} = \mathbf{M}^{-1} \mathbf{f}(\mathbf{x}, t)$$

# Semi-explicit DAEs

- Write stirred tank example 2 in semi-explicit form:



$$\frac{dc_2}{dt} = \frac{Q}{V} (c_1(t) - c_2(t))$$

$$c_2(t) = \gamma(t)$$

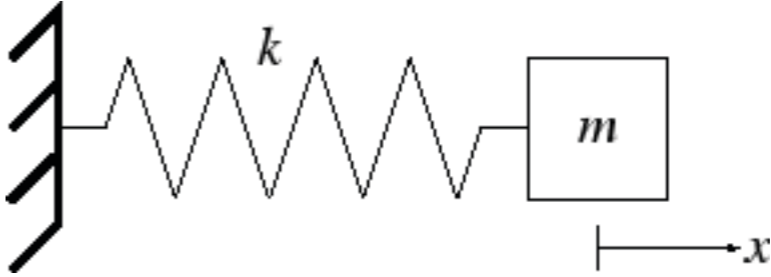
# Semi-explicit DAEs

- Problems of the sort:  $\mathbf{M} \frac{d\mathbf{x}}{dt} = \mathbf{f}(\mathbf{x}, t), \mathbf{x}(0) = \mathbf{x}_0$
- $\mathbf{M}$  is called the “mass matrix”
- Many semi-explicit DAEs can be written in the simplified form:

$$\begin{aligned} \frac{d\mathbf{x}}{dt} &= \mathbf{f}(\mathbf{x}, \mathbf{y}, t) & \mathbf{x}(0) &= \mathbf{x}_0 \\ 0 &= \mathbf{g}(\mathbf{x}, \mathbf{y}, t) & 0 &= \mathbf{g}(\mathbf{x}_0, \mathbf{y}(0), t) \end{aligned}$$

- where
  - $\mathbf{x}$  are called the differential states
  - $\mathbf{y}$  are called the algebraic states

# Fully implicit DAEs

- Example: mass-spring system 
- Conservation of energy:  $E = \frac{1}{2}m(\dot{x})^2 + \frac{1}{2}kx^2$

$$f(x, \dot{x}, t) = \frac{1}{2}m(\dot{x})^2 + \frac{1}{2}kx^2 - E = 0$$

has a solution:

$$x = a \cos(\omega t)$$

$$\frac{1}{2}ma^2\omega^2 \sin^2(\omega t) + \frac{1}{2}ka^2 \cos^2(\omega t) = E$$

$$\omega = \sqrt{\frac{k}{m}}, \quad a = \sqrt{\frac{E}{k}}$$



# Fully implicit DAEs

- Many problems contain non-linearities with respect to differentials of the state variables.  $\mathbf{f}(\mathbf{x}, \dot{\mathbf{x}}, t) = 0$ ,  $\mathbf{x}(0) = \mathbf{x}_0$

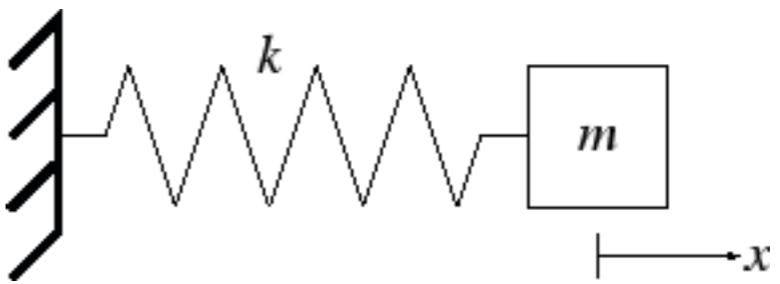
- If  $\left. \frac{\partial \mathbf{f}}{\partial \dot{\mathbf{x}}} \right|_{t, \mathbf{x}}$  is full rank, then the DAE can be represented as an equivalent ODE:

$$d\mathbf{f} = \left. \frac{\partial \mathbf{f}}{\partial \dot{\mathbf{x}}} \right|_{t, \mathbf{x}} d\dot{\mathbf{x}} + \left. \frac{\partial \mathbf{f}}{\partial \mathbf{x}} \right|_{t, \dot{\mathbf{x}}} d\mathbf{x} + \left. \frac{\partial \mathbf{f}}{\partial t} \right|_{\mathbf{x}, \dot{\mathbf{x}}} dt = 0$$



$$\frac{d\dot{\mathbf{x}}}{dt} = - \left( \left. \frac{\partial \mathbf{f}}{\partial \dot{\mathbf{x}}} \right|_{t, \mathbf{x}} \right)^{-1} \left( \left. \frac{\partial \mathbf{f}}{\partial \mathbf{x}} \right|_{t, \dot{\mathbf{x}}} \frac{d\mathbf{x}}{dt} + \left. \frac{\partial \mathbf{f}}{\partial t} \right|_{\mathbf{x}, \dot{\mathbf{x}}} \right) = 0$$

# Fully implicit DAEs

- Example: mass-spring system 

- Conservation of energy:  $E = \frac{1}{2}m(\dot{x})^2 + \frac{1}{2}kx^2$

$$f(x, \dot{x}, t) = \frac{1}{2}m(\dot{x})^2 + \frac{1}{2}kx^2 - E = 0$$

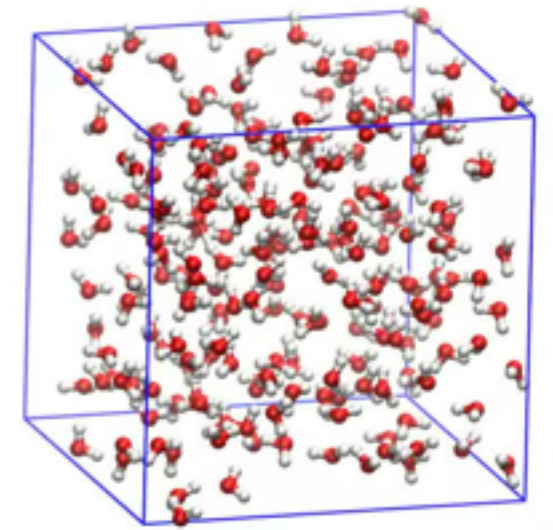
transform to ODE

$$\frac{\partial f}{\partial \dot{x}} = m\dot{x}, \quad \frac{\partial f}{\partial x} = kx, \quad \frac{\partial f}{\partial t} = 0$$

↓

$$\ddot{x} = -\frac{k}{m}x$$

# Fully implicit DAEs



- Example: molecular dynamics

- Conservation of energy:  $E = \frac{1}{2}m\|\dot{\mathbf{x}}\|_2^2 + V(\mathbf{x})$

$$f(\dot{\mathbf{x}}, \mathbf{x}, t) = \frac{1}{2}m\|\dot{\mathbf{x}}\|_2^2 + V(\mathbf{x}) - E$$



$$df = \left. \frac{\partial f}{\partial \dot{\mathbf{x}}} \right|_{t, \mathbf{x}} d\dot{\mathbf{x}} + \left. \frac{\partial f}{\partial \mathbf{x}} \right|_{t, \dot{\mathbf{x}}} d\mathbf{x} + \left. \frac{\partial f}{\partial t} \right|_{\mathbf{x}, \dot{\mathbf{x}}} dt = 0$$

↓  $\frac{\partial f}{\partial \dot{\mathbf{x}}} = m\dot{\mathbf{x}}$

$$0 = \dot{\mathbf{x}} \cdot (m\ddot{\mathbf{x}} + \nabla V(\mathbf{x}))$$

- Symplectic integrators used to integrate equations of motion while exerting control over error in the total energy.

# Numerical Simulation of DAEs

- Consider the semi-explicit DAE:

$$\begin{aligned}\frac{d\mathbf{x}}{dt} &= \mathbf{f}(\mathbf{x}, \mathbf{y}, t) & \mathbf{x}(0) &= \mathbf{x}_0 \\ 0 &= \mathbf{g}(\mathbf{x}, \mathbf{y}, t)\end{aligned}$$

- Consider applying the forward Euler approximation:

$$\begin{aligned}\mathbf{x}(t + \Delta t) - \mathbf{x}(t) &= \Delta t \mathbf{f}(\mathbf{x}(t), \mathbf{y}(t), t) \\ 0 &= \mathbf{g}(\mathbf{x}(t), \mathbf{y}(t), t)\end{aligned}$$

- Determining the algebraic states always requires solution of a nonlinear equation.
- DAE simulation methods are inherently implicit.

# Numerical Simulation of DAEs

- Consider the fully implicit DAE:

$$\mathbf{f}(\mathbf{x}, \dot{\mathbf{x}}, t) = 0, \quad \mathbf{x}(0) = \mathbf{x}_0$$

- No way in general to avoid solving systems of nonlinear equations.
- Backward difference approximations for  $\dot{\mathbf{x}}$  are substituted and time marching solutions determined.
- Example, backward Euler approximation:

$$\text{solve: } \mathbf{f} \left( \mathbf{x}(t_k), \frac{\mathbf{x}(t_k) - \mathbf{x}(t_{k-1})}{t_k - t_{k-1}}, t_k \right) = 0 \quad \text{for: } \mathbf{x}(t_k)$$

$$\text{solve: } \mathbf{f} \left( \mathbf{x}(t_{k+1}), \frac{\mathbf{x}(t_{k+1}) - \mathbf{x}(t_k)}{t_{k+1} - t_k}, t_{k+1} \right) = 0 \quad \text{for: } \mathbf{x}(t_{k+1})$$

# Numerical Simulation of DAEs

- Consider the semi-explicit DAE:

$$\frac{d\mathbf{x}}{dt} = \mathbf{f}(\mathbf{x}, \mathbf{y}, t) \quad \mathbf{x}(0) = \mathbf{x}_0$$
$$0 = \mathbf{g}(\mathbf{x}, \mathbf{y}, t)$$

- No way in general to avoid solving systems of nonlinear equations.
- Backward difference approximations for  $\dot{\mathbf{x}}$  are substituted and time marching solutions determined.
- Example, backward Euler approximation:

solve:  $0 = \frac{\mathbf{x}(t_k) - \mathbf{x}(t_{k-1})}{t_k - t_{k-1}} - \mathbf{f}(\mathbf{x}(t_k), \mathbf{y}(t_k), t_k)$  for:  $\mathbf{x}(t_k)$

$$0 = \mathbf{g}(\mathbf{x}(t_k), \mathbf{y}(t_k), t_k)$$

# Numerical Simulation of DAEs

- How suitable are such approaches?
- Consider stirred tank example I:

$$\frac{dc_2}{dt} = \frac{Q}{V} (c_1(t) - c_2(t))$$
$$c_1(t) = \gamma(t)$$

Apply backward Euler method:

$$c_1(t_k) = \gamma(t_k)$$

$$c_2(t_k) = \frac{1}{1 + \frac{Q}{V}(t_k - t_{k-1})} \left( c_2(t_{k-1}) + \frac{Q}{V}(t_k - t_{k-1})c_1(t_k) \right) + O((t_k - t_{k-1})^2)$$

# Numerical Simulation of DAEs

- How suitable are such approaches?
- Consider stirred tank example 2:

$$\frac{dc_2}{dt} = \frac{Q}{V} (c_1(t) - c_2(t))$$
$$c_2(t) = \gamma(t)$$

Apply backward Euler method:

$$c_2(t_k) = \gamma(t_k)$$

$$c_1(t_k) = c_2(t_k) + \frac{V}{Q} \left( \frac{c_2(t_k) - c_2(t_{k-1})}{t_k - t_{k-1}} \right) + O(t_k - t_{k-1})$$



# Numerical Simulation of DAEs

- How suitable are such approaches?
- Consider the system of DAEs:

$$\dot{c}_2 = c_1(t)$$

$$\dot{c}_3 = c_2(t)$$

$$0 = c_3(t) - \gamma(t)$$

What is the exact solution?

Apply backward Euler method:

$$c_3(t_k) = \gamma(t_k)$$

$$c_2(t_k) = \frac{c_3(t_k) - c_3(t_{k-1})}{t_k - t_{k-1}} + O(t_k - t_{k-1})$$

$$c_1(t_k) = \frac{c_2(t_k) - c_2(t_{k-1})}{t_k - t_{k-1}} + O(1)!$$

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