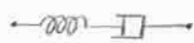


Last time = - models of viscoelastic behavior (Maxwell, Voigt, SLS), creep & stress relaxation
 - oscillatory behavior

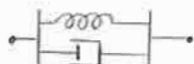
Today - applications of lumped models
 - generalized LV descriptions
 - continuum LV descriptions

Lumped models

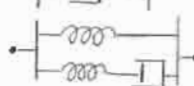
Maxwell



Voigt



SLS



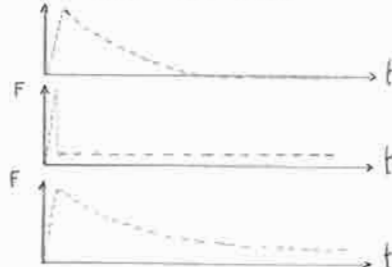
Generalized equations

$$\frac{du}{dt} = \frac{1}{k} \frac{dF}{dt} + \frac{F}{\eta}$$

$$F = \eta \frac{du}{dt} + k u$$

$$F + \alpha \frac{dF}{dt} = k_1 u + \beta \frac{du}{dt}$$

Stress relaxation



• data don't fit \Rightarrow add elements

Oscillatory motion

$$u(t) = u_0 \cos(\omega t) = \text{Re} [u_0 \exp(i\omega t)]$$

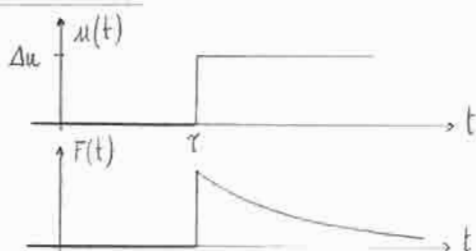
$$F(t) = F_0 \cos(\omega t + \phi) = \text{Re} [F_0 \exp(i(\omega t + \phi))] \quad \text{and}$$

$$\left\{ \begin{array}{l} \text{storage modulus } G'(\omega) = \frac{F_0(\omega)}{u_0} \cos \phi \\ \text{loss modulus } G''(\omega) = \frac{F_0(\omega)}{u_0} \sin \phi \end{array} \right.$$

steady-state behavior

Generalized linear viscoelastic models

Consider the experiment



In general, let $F(t) = g(t-\tau) \Delta u(\tau)$

linear \Rightarrow superposition $F(t) = \sum_i g_i(t-\tau_i) \Delta u(\tau_i)$

limit of a smooth $u(t)$: $F(t) = \int_{-\infty}^t g(t-\tau) \frac{du(\tau)}{d\tau} d\tau$

\hookrightarrow relaxation function (see chapter 1 - Ferry)

We want



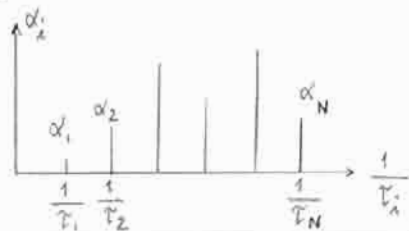
general representation (many lumped elements)

(recall for Maxwell

$$F(t) = k u_0 \exp\left(-\frac{t}{\tau_R}\right), \quad \tau_R = \eta/k$$

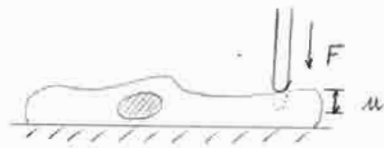
$$u(t) = \sum_{i=0}^N \alpha_i \exp\left(-\frac{t}{\tau_i}\right)$$

• discrete



or continuous





single force & single displacement
but nonhomogeneous, anisotropic,
complex composition & structure

Lumped model \rightarrow continuum description

lumped parameter $F(t) = \int_{-\infty}^t g(t-\tau) \frac{du(\tau)}{d\tau} d\tau$

continuum
(see Ferry)

$$\sigma_{ij}(\bar{x}, t) = 2 \int_{-\infty}^t G_{ijkl}(\bar{x}, t-\tau) \frac{d\epsilon_{kl}}{d\tau} d\tau$$

\rightarrow tensorial relaxation function

and for viscoelastic fluid

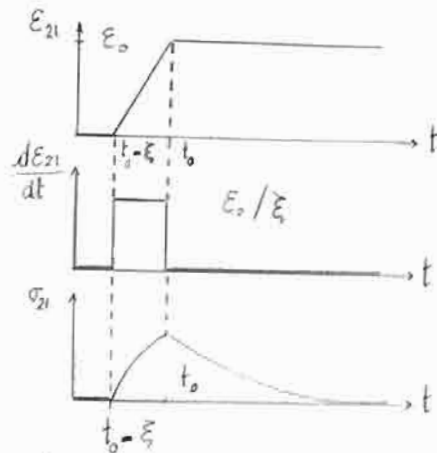
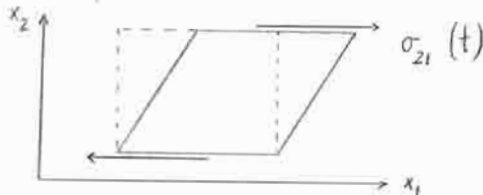
$$\sigma_{ij} = 2 \int_{-\infty}^t \frac{dG_{ijkl}(\bar{x}, t-\tau)}{d\tau} \epsilon_{kl}(t, \tau) d\tau$$

\rightarrow strain at t relative to strain at τ

What is the relationship between G_{ijkl} and G ?

\rightarrow shear modulus

linear pure shear deformation



$$\begin{aligned} \sigma_{21}(t) &= 2 \int_{-\infty}^t G(t-\tau) \frac{d\epsilon_{21}(\tau)}{d\tau} d\tau \\ &= 2 \int_{t_0-\xi}^{t_0} G(t-\tau) \frac{\epsilon_0}{\xi} d\tau \quad \text{for } t \gg t_0 \\ &= 2 G(t - (t_0 + \xi \delta)) \frac{\epsilon_0}{\xi} \quad , \quad 0 \leq \delta \leq 1 \end{aligned}$$

for $\xi \ll t$ and $t_0 = 0$, we have

$$\sigma_{21}(t) = 2 G(t) \epsilon_0$$

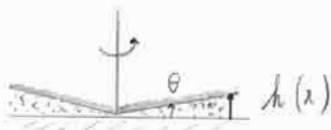
linear viscoelastic solid

$$\sigma_{21} = 2G \epsilon_{21}$$

linear elastic solid

$G(t)$ not to be confused with $G'(\omega)$ or $G''(\omega)$

ex. cone-plate rheometer



top view



side view



impose oscillatory shear $\epsilon_{21} = \frac{1}{2} \frac{\partial u_1}{\partial x_2} = \frac{1}{2} \cdot \frac{\pi \gamma}{\pi \theta} = \frac{\gamma}{2\theta}$ independent of radius.

measure torque $T = \int_0^R \sigma_{21} \cdot 2\pi r \cdot dr = 2\pi \sigma_{21} \frac{R^3}{3}$

$$\sigma_{21}(t) = \frac{3}{2\pi} \cdot \frac{T}{R^3}$$

because T measurable, $\sigma_{21}(t)$ is, too

recall $\hat{G}(\omega) = \frac{\hat{F}(\omega)}{\hat{u}_0} = G' + i G''$

or continuum $\hat{G}(\omega) = \frac{\hat{\sigma}_{21}(\omega)}{2\hat{\epsilon}_{21}} = \frac{\sigma_0 \exp(i\phi)}{2\epsilon_0}$ because $\hat{\sigma}_{21} = \sigma_0 \exp(i(\omega t + \phi))$
 $\hat{\epsilon}_{21} = \epsilon_0 \exp(i\omega t)$

$$\hat{G}(\omega) = \frac{\sigma_0}{2\epsilon_0} (\cos \phi + i \sin \phi)$$

$$= \underbrace{\frac{\sigma_0}{2\epsilon_0} \cos \phi}_{G'} + i \underbrace{\frac{\sigma_0}{2\epsilon_0} \sin \phi}_{G''}$$

- look at before gelation



viscous liquid

after gelation



elastic

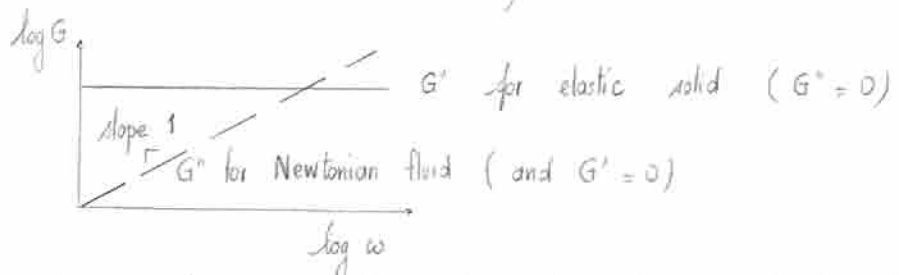
- limiting cases

$$\hat{G}(\omega) = \frac{\sigma_0}{2\epsilon_0} \cos \phi + i \frac{\sigma_0}{2\epsilon_0} \sin \phi$$

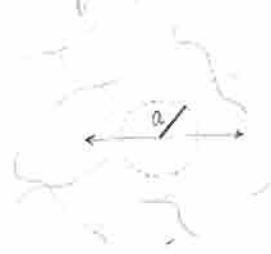
elastic solid $\phi \rightarrow 0$ $\hat{G} = \frac{\sigma_0}{2\epsilon_0} = G'$ real and $G'' = 0$

viscous liquid $\phi \rightarrow \frac{\pi}{2}$ $\hat{G} = i \frac{\sigma_0}{2\epsilon_0} = i G''$ pure imaginary and $G' = 0$

Newtonian fluid $\sigma_{21} = 2\mu \frac{d\epsilon_{21}}{dt} = -2 \underbrace{\mu}_{\sigma_0} \epsilon_0 \omega \sin(\omega t)$ and $G'' = \frac{2\mu \epsilon_0 \omega}{2\epsilon_0}$
 $G''(\omega) = \mu \omega$



. Oscillating sphere inside an infinite viscoelastic medium (Zieman et al 1984, Sackmann group)



$u(t), F(t)$
 bead in medium $\left\{ \begin{array}{l} \text{isotropic} \\ \text{homogeneous} \\ \text{linearly viscoelastic} \end{array} \right.$

$u = u_0 \cos(\omega t)$
 $F = F_0 \cos(\omega t + \phi)$
 superimpose F_v & F_e defined as follows

- if $\left\{ \begin{array}{l} \text{purely viscous} \\ \text{Newtonian} \\ \text{no inertia} \end{array} \right.$ Stokes flow
- if purely elastic

$$F_v(t) = 6\pi \mu a \frac{du}{dt}$$

↑
coefficient of viscosity

$$F_e(t) = 6\pi G a u$$