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## Lecture 26 The Clohessy-Wiltshire Equations of Relative Motion

### Clohessy-Wiltshire Equations †

We begin with the equations for the restricted three-body problem

$$m \left[ \frac{d^2 \mathbf{r}}{dt^2} + 2\boldsymbol{\omega} \times \frac{d\mathbf{r}}{dt} + \boldsymbol{\omega} \times (\boldsymbol{\omega} \times \mathbf{r}) \right] = -\frac{Gmm_1}{\rho_1^3} \boldsymbol{\rho}_1 - \frac{Gmm_2}{\rho_2^3} \boldsymbol{\rho}_2$$

where

$$\begin{aligned} \boldsymbol{\rho}_1 &= \mathbf{r} - \mathbf{r}_1 & \boldsymbol{\rho}_2 &= \mathbf{r} - \mathbf{r}_2 & \mathbf{r} &= \mathbf{r}_3 - \frac{m_1 \mathbf{r}_1 + m_2 \mathbf{r}_2}{m_1 + m_2} \\ \boldsymbol{\omega} &= \omega \mathbf{i}_\zeta & \text{with } \omega^2 &= \frac{G(m_1 + m_2 + m)}{r_{12}^3} \approx \frac{G(m_1 + m_2)}{r_{12}^3} \end{aligned}$$

With  $m_1$  and  $m_2$  on  $\xi$ -axis, then  $\mathbf{r}_1 = r_1 \mathbf{i}_\xi$  and  $\mathbf{r}_2 = r_2 \mathbf{i}_\xi$

To adapt these equations to the problem of a chase spacecraft  $m$  in pursuit of a target spacecraft  $m_1$  both moving about a central body of mass  $m_2$ , let both  $m$  and  $m_1$  become infinitesimal. As a result  $r_2$  will be zero so that  $\mathbf{r}$  and  $\boldsymbol{\rho}_2$  are the same vector. The vector  $\boldsymbol{\rho}_1 \equiv \boldsymbol{\rho}$  is the position of the chase spacecraft relative to the target spacecraft. Further, the angular velocity is

$$\omega^2 = \frac{Gm_2}{r_1^3} \quad \text{or} \quad \omega^2 r_1^3 = Gm_2$$

so that the equations of motion of the chase spacecraft can be written as

$$\frac{d^2 \boldsymbol{\rho}}{dt^2} + 2\boldsymbol{\omega} \times \frac{d\boldsymbol{\rho}}{dt} + \boldsymbol{\omega} \times [\boldsymbol{\omega} \times (\boldsymbol{\rho} + \mathbf{r}_1)] = -\frac{\omega^2 r_1^3}{r^3} \mathbf{r}$$

where  $\boldsymbol{\rho}$  and  $\mathbf{r}_1 = r_1 \mathbf{i}_\xi$  are the position vectors of the chase and target spacecrafts, respectively.

**Note:**  $\mathbf{r} = \boldsymbol{\rho} + \mathbf{r}_1$

This differential equation is non-linear because of the factor  $1/r^3$ . However, with the use of the Taylor Series expansion, we write

$$\begin{aligned} \frac{r^2}{r_1^2} &= \frac{(\boldsymbol{\rho} + \mathbf{r}_1) \cdot (\boldsymbol{\rho} + \mathbf{r}_1)}{r_1^2} = \frac{\rho^2 + 2\boldsymbol{\rho} \cdot \mathbf{r}_1 + r_1^2}{r_1^2} = 1 + 2x \mathbf{i}_\xi \cdot \mathbf{i}_{r_1} + x^2 \\ \frac{r_1}{r} &= (1 + 2\mathbf{i}_\xi \cdot \mathbf{i}_{r_1} x + x^2)^{-\frac{1}{2}} = 1 - \mathbf{i}_\xi \cdot \mathbf{i}_{r_1} x + \dots \end{aligned}$$

where  $x = \frac{\rho}{r_1}$ . Therefore,

$$\frac{r_1^3}{r^3} = 1 - 3\mathbf{i}_\xi \cdot \mathbf{i}_\rho \frac{\rho}{r_1} + O\left(\frac{\rho^2}{r_1^2}\right)$$

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† W.H. Clohessy and R.S. Wiltshire, Journal of Aerospace Sciences, Vol. 27, No. 9, 1960, pp. 653–658.

and the equation will be linear if we ignore the higher order terms. Then

$$\frac{d^2 \boldsymbol{\rho}}{dt^2} + 2\boldsymbol{\omega} \times \frac{d\boldsymbol{\rho}}{dt} + \boldsymbol{\omega} \times [\boldsymbol{\omega} \times (\boldsymbol{\rho} + \mathbf{r}_1)] = -\omega^2 \left[ 1 - 3(\mathbf{i}_\xi \cdot \boldsymbol{\rho}) \frac{1}{r_1} \right] (\boldsymbol{\rho} + \mathbf{r}_1)$$

reduces to

$$\frac{d^2 \boldsymbol{\rho}}{dt^2} + 2\boldsymbol{\omega} \times \frac{d\boldsymbol{\rho}}{dt} + \boldsymbol{\omega} \times (\boldsymbol{\omega} \times \boldsymbol{\rho}) = -\omega^2 \boldsymbol{\rho} + 3\omega^2 (\mathbf{i}_\xi \cdot \boldsymbol{\rho}) \mathbf{i}_\xi + O(\rho^2)$$

since the term with the factor  $(\mathbf{i}_\xi \cdot \boldsymbol{\rho}) \boldsymbol{\rho}$  is  $O(\rho^2)$ .

Finally,

$$\boldsymbol{\rho} = \xi \mathbf{i}_\xi + \eta \mathbf{i}_\eta + \zeta \mathbf{i}_\zeta$$

so that

$$\boldsymbol{\omega} \times (\boldsymbol{\omega} \times \boldsymbol{\rho}) = -\omega^2 (\xi \mathbf{i}_\xi + \eta \mathbf{i}_\eta) \quad \text{and} \quad \mathbf{i}_\xi \cdot \boldsymbol{\rho} = \xi$$

Therefore, the differential equation for **the motion of the chase spacecraft relative to the target spacecraft** is

$$\boxed{\frac{d^2 \boldsymbol{\rho}}{dt^2} + 2\boldsymbol{\omega} \times \frac{d\boldsymbol{\rho}}{dt} = -\omega^2 \zeta \mathbf{i}_\zeta + 3\omega^2 \xi \mathbf{i}_\xi + O(\rho^2)}$$

or in scalar form

$$\boxed{\begin{aligned} \frac{d^2 \xi}{dt^2} - 2\omega \frac{d\eta}{dt} - 3\omega^2 \xi &= 0 \\ \frac{d^2 \eta}{dt^2} + 2\omega \frac{d\xi}{dt} &= 0 \\ \frac{d^2 \zeta}{dt^2} + \omega^2 \zeta &= 0 \end{aligned}}$$

It is sometimes convenient to express the position vector

$$\boldsymbol{\rho} \equiv \mathbf{r} = x \mathbf{i}_\theta + y \mathbf{i}_r - z \mathbf{i}_z \quad \mathbf{i}_{r_1} = \mathbf{i}_r \quad \boldsymbol{\omega} = -\omega \mathbf{i}_z$$

with  $x$  in the direction of motion  $\mathbf{i}_\theta$ ,  $y$  in the radial direction  $\mathbf{i}_r$ , and  $\mathbf{i}_z = \mathbf{i}_\theta \times \mathbf{i}_r$  normal to the orbital plane. Then the equations of motion are<sup>‡</sup> are

$$\boxed{\begin{aligned} \frac{d^2 x}{dt^2} + 2\omega \frac{dy}{dt} &= 0 \\ \frac{d^2 y}{dt^2} - 2\omega \frac{dx}{dt} - 3\omega^2 y &= 0 \\ \frac{d^2 z}{dt^2} + \omega^2 z &= 0 \end{aligned}}$$

The Clohessy-Wiltshire equations are three simultaneous second-order, linear, constant-coefficient, coupled differential equations which are capable of exact solution.

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<sup>‡</sup> S.W. Shepperd, Journal of Guidance, Control, and Dynamics, Vol. 14, No. 6, 1991, pp. 1318–1322.

## General Solution of the C-W Equations

Introduce the dimensionless time variable  $\tau = \omega t$  so that the Clohessy-Wiltshire equations take the form

$$\begin{aligned}\frac{d^2x}{d\tau^2} + 2\frac{dy}{d\tau} &= 0 \\ \frac{d^2y}{d\tau^2} - 2\frac{dx}{d\tau} - 3y &= 0 \\ \frac{d^2z}{d\tau^2} + z &= 0\end{aligned}$$

The general solution of these equations, with initial conditions  $x_0, y_0, z_0, \dot{x}_0, \dot{y}_0$  and  $\dot{z}_0$  and using the notation  $\frac{dx}{d\tau} = \dot{x}$ ,  $\frac{dy}{d\tau} = \dot{y}$  and  $\frac{dz}{d\tau} = \dot{z}$ , is

$$\begin{aligned}\begin{bmatrix} x \\ y \\ \dot{x} \\ \dot{y} \end{bmatrix} &= \begin{bmatrix} 1 & 6\sin\tau - 6\tau & 4\sin\tau - 3\tau & 2\cos\tau - 2 \\ 0 & 4 - 3\cos\tau & 2 - 2\cos\tau & \sin\tau \\ 0 & 6\cos\tau - 6 & 4\cos\tau - 3 & -2\sin\tau \\ 0 & 3\sin\tau & 2\sin\tau & \cos\tau \end{bmatrix} \begin{bmatrix} x_0 \\ y_0 \\ \dot{x}_0 \\ \dot{y}_0 \end{bmatrix} \\ \begin{bmatrix} z \\ \dot{z} \end{bmatrix} &= \begin{bmatrix} \cos\tau & \sin\tau \\ -\sin\tau & \cos\tau \end{bmatrix} \begin{bmatrix} z_0 \\ \dot{z}_0 \end{bmatrix}\end{aligned}$$