

Turbulent Shear layers.

7.1 > B) Prandtl's Analogy

7.2 > A) Turbulent BL structure

B) Effect of Roughness

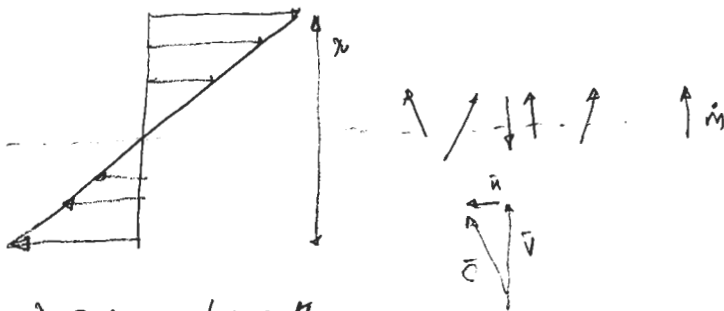
Reading: Sch 495 - 552  
 EPB 160 - 210  
 ASL 394 - 449.

7.1 D) Prandtl's Analogy. (with kinetic theory)

From last class.

$$\frac{\partial \bar{u}}{\partial t} = -\frac{1}{\rho} \frac{\partial}{\partial x} (\bar{p} + \rho \bar{u}'^2) + \underbrace{\frac{\partial}{\partial y} (\rho \bar{u}' v') - \rho \bar{u}' v'}_{\tau} - 2D \text{ X-mom} \quad \text{TSL}$$

Molecular level



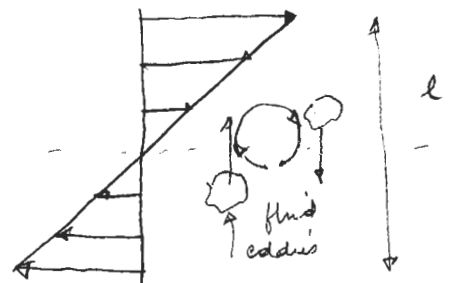
$\lambda = \text{mean free path}$

$\bar{c} = \text{molecular speed}$

X-mom flux:  $\rho \bar{u}' \bar{u} = \rho \bar{v}' \bar{u} = \rho \bar{v}' \frac{\lambda}{2} \frac{du}{dy}$   
 $\approx \underbrace{\rho \bar{c}}_M \frac{\lambda}{2} \frac{du}{dy}$

Y-mom flux:  $\rho \bar{u}' \bar{v}' \approx \rho \bar{c}^2$

Macroscopic level

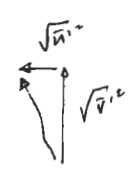


$l = \text{mixing length}$

$\tau_{\text{turb}} = -\rho \bar{u}' v'$

$\rho \bar{u}' \bar{v}' \approx \rho \bar{u}'^2$

$\sqrt{\bar{u}'^2} \approx \sqrt{\bar{v}'^2}$



Similar to laminar (molecular level)  
Analogous:

$$|\bar{u}'| = l \left| \frac{d\bar{u}}{dy} \right|$$

Since  $v' \sim u'$  magnitude

$$|\bar{v}'| = \text{const.} |\bar{u}'| = \text{const.} l \left| \frac{d\bar{u}}{dy} \right|$$

Approximate

$$\bar{u}'v' = -c |\bar{u}'| |\bar{v}'| \quad 0 < c < 1 \quad (\text{constant})$$

$$\therefore \bar{u}'v' = -\text{const} l^2 \left( \frac{d\bar{u}}{dy} \right)^2$$

$$\therefore \tau_t = -\rho \bar{u}'v' = \rho l^2 \left( \frac{d\bar{u}}{dy} \right)^2$$

Where  $l$  is an unknown mixing length  $l_m$  (absorb constants)

A more correct way is to write

$$\tau_t = \rho l^2 \left| \frac{d\bar{u}}{dy} \right| \left( \frac{d\bar{u}}{dy} \right)$$

since  $\tau_t$  can change sign with  $\frac{d\bar{u}}{dy}$ .

Comparing with Prandtl's hypothesis

$$\tau_t = M_t \frac{d\bar{u}}{dy}$$

we get

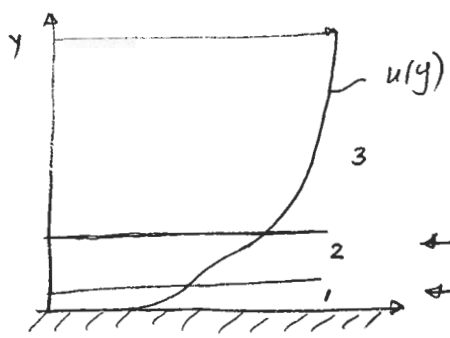
$$M_t = \rho l^2 \left| \frac{d\bar{u}}{dy} \right|$$

$$\text{or } \nu_t = l^2 \left| \frac{d\bar{u}}{dy} \right| \quad - \text{Mixing length model}$$

Complete if we can relate  $l$  to the flow.

7.27 A) Turbulent BL structure

Turbulent wall BL has 3 distinct layers (emp. fact)

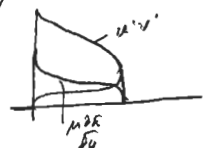


wake / outlet layer } outer  
 log layer } wall layer  
 laminar sublayer } inner

unlike laminar scales

- \* Inner layer - viscous shear ( $\mu$  molecular) dominates
- \* Outer layer - turbulent shear dominates

In the inner layer



Inner layer retards outer wake layer

$$u = f(\underbrace{\tau_w, \rho, \mu}_{\text{physical param.}}, y, \underbrace{k}_{\text{roughness height}})$$

- function of depend

Velocity scale:

$$u_c = \sqrt{\frac{\tau_w}{\rho}} = u^* \quad (\text{shear velocity}) \quad (10 \frac{u_c}{s})$$

Length scale:

$$l_c = \frac{\mu}{\sqrt{\rho \tau_w}} = \frac{\nu}{u^*} = l^*$$

Non-dimensional dep:

$$\frac{u}{u^*} = f\left(\frac{y}{l^*}, \frac{k}{l^*}\right)$$

$$\frac{y}{l^*} = y^+, \quad \frac{u}{u^*} = u^+ \quad (\text{non variables})$$

In outer layer: velocity scale  $u_c - u$

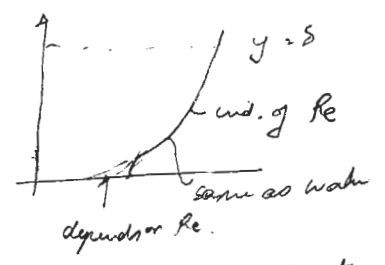
defect law  $\rightarrow u_c - \bar{u} = f\left(y, \rho, \tau_w, \delta^*, \frac{d\rho}{dx}\right)$

Length scale :  $\delta$  or  $\delta^*$

Non-dimension :

$$\frac{u_e - \bar{u}}{u^*} = \frac{g}{f} \left( y/\delta^* \right) \left[ \frac{\delta^*}{\tau_w} \frac{dp}{dx} \right]$$

$\downarrow$   $\tau_w$  shear stress  
 $\downarrow$   $\frac{dp}{dx}$  non-dimensional pressure gradient



velocity effect is dependant variable

We can develop velocity profile

① Sublayer

$$u^+ = u/u^* \quad y^+ = y/L^* \quad \therefore \mu \frac{\partial u}{\partial y} = \tau_w \Rightarrow \frac{\partial u^+}{\partial y^+} = 1$$

$\therefore \boxed{u^+ = y^+}$  in viscous sublayer

② overlap / log layer

$$u^+ = f(y^+) = f\left(\left(\frac{\delta^*}{2}\right) \cdot (y/\delta)\right) = \frac{u_e}{u^*} - g(y/\delta)$$

f contains multiplicative const, g an additive const.

$\Rightarrow$  f and g are logarithmic

$$u^+ = \frac{1}{k} \ln y^+ + B$$

$$\frac{u_e - u}{u^*} = -\frac{1}{k} \ln (y/\delta) + A$$

$\uparrow$  depends on  $\frac{dp}{dx}$

A other approach:  $l = ky$  (mixing length)

$$\tau = \rho l^2 \left(\frac{\partial \bar{u}}{\partial y}\right)^2 = \rho k^2 L^2 \left(\frac{\partial \bar{u}}{\partial y}\right)^2$$

Near the wall:  $\tau = \tau_w \rightarrow \tau_w/\rho = u^{*2} = k^2 y^2 \left(\frac{\partial \bar{u}}{\partial y}\right)^2$

# Integrating

$$\bar{u} = \frac{u^*}{k} \ln y + C$$

(y<sup>+</sup>)

At y = δ      $\bar{u} = u_c$

$$\therefore \frac{\bar{u} - u_c}{u^*} = -\frac{1}{k} \ln(y/\delta) \quad (0 \text{ pressure gradient})$$

