

**16.100 Homework Assignment #2**  
Due: Wednesday, September 21<sup>th</sup>, 9am

**Reading Assignment**

Anderson, 3<sup>rd</sup> edition: Chapter 2, Sections 2.4-2.6, 2.10  
Chapter 3, Sections 3.1-3.2, 3.5-3.16

**Problem 1 (30%)**

**Useful reading:** Sections 2.10, 3.6 of Anderson

The incompressible, inviscid flow equations (called the incompressible Euler equations) are:

$$\nabla \cdot \vec{V} = 0 \quad (\text{Eq. 1})$$

$$\rho \frac{D\vec{V}}{Dt} = -\nabla p \quad (\text{Eq. 2})$$

- a) Starting from the incompressible Euler equations, derive the following ‘Bernoulli-like’ equation:

$$\rho \frac{\partial \vec{V}}{\partial t} + \nabla \left( p + \frac{1}{2} \rho |\vec{V}|^2 \right) = \rho \vec{V} \times \vec{\omega}$$

where  $\vec{\omega} = \nabla \times \vec{V}$  is the vorticity. The following vector calculus identity might be helpful:

$$(\vec{V} \cdot \nabla) \vec{V} = \nabla \left( \frac{1}{2} |\vec{V}|^2 \right) - \vec{V} \times \vec{\omega}$$

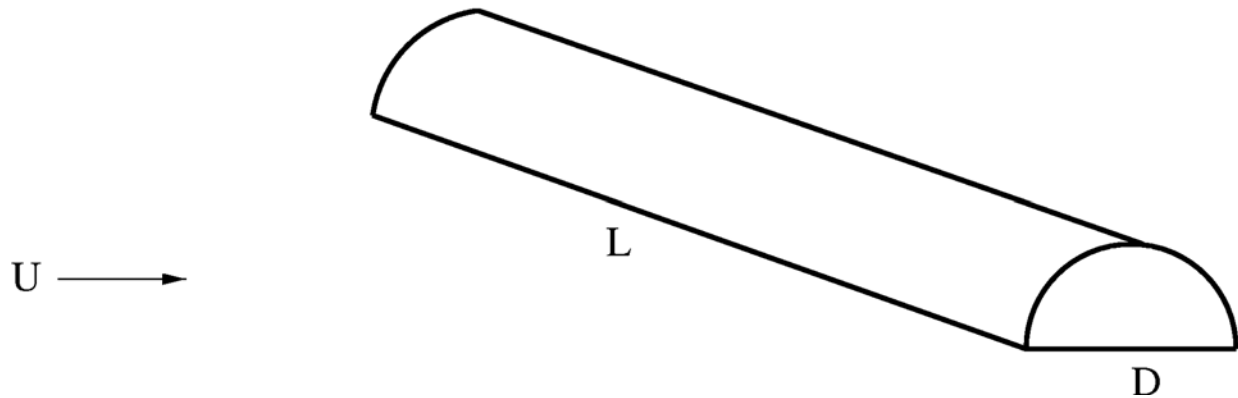
- b) Show that the total pressure,  $p + \frac{1}{2} \rho |\vec{V}|^2$ , is constant along a streamline in a steady, inviscid flow.
- c) Show that the total pressure is constant everywhere in a steady, inviscid, and irrotational flow.
- d) By taking the curl of the incompressible, inviscid momentum equation (Eq. 2 above), show that:

$$\frac{D\vec{\omega}}{Dt} = \vec{\omega} \cdot \nabla \vec{V}$$

- e) If the vorticity of a fluid element is  $\vec{\omega}_0$  at time  $t = 0$  and the flow is two-dimensional, prove that the vorticity is always equal to  $\vec{\omega}_0$  for any  $t > 0$ .

**Problem 2 (40%)**

**Useful reading:** Section 3.13 of Anderson

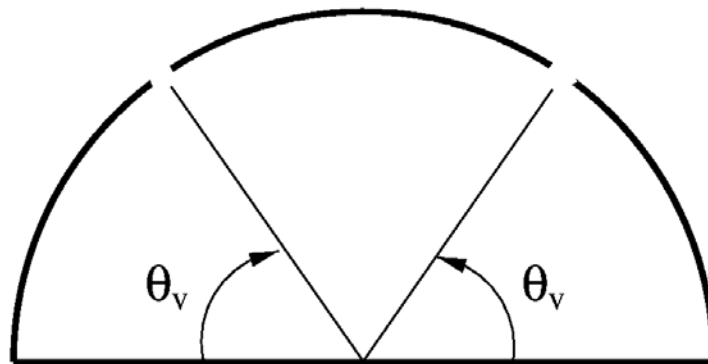


Consider the semi-cylinder aircraft hangar shown above. Assume:

- Far upstream of the hangar, the wind has uniform speed  $U$  and is perpendicular to the hangar length. The upstream pressure is  $p_\infty$ .
- The end effects are small.
- The flow is inviscid to good approximation.

Answer the following questions:

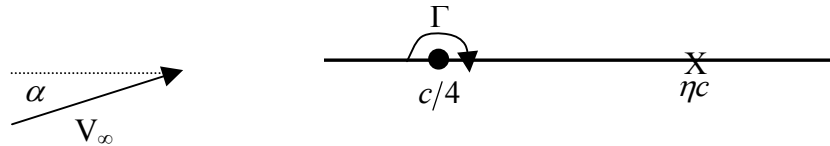
- a) Assume the pressure in the interior of the hangar is  $p_H$ . If the circular roof can withstand a maximum net vertical force of  $F_{\max}$ , what is the maximum velocity the hangar can withstand?
- b) To reduce the pressure differential between the inside and outside of the hangar, vents are to be placed at positions  $\theta_v$  as shown in the figure below. When this is done, the pressure inside the hangar will be equal to the pressure outside the hangar at the vent location. What should  $\theta_v$  be to make the net vertical force on the roof zero?



**Problem 3 (30%)**

**Useful reading:** Section 3.7, 3.14, 3.16 of Anderson

A simple model for a thin, symmetric airfoil (i.e. no camber) is to place a point vortex at the quarter-chord location and then satisfy flow tangency at a selected control point located on the chord line at  $\eta c$  as shown in the figure below.



Thin airfoil theory gives that the lift coefficient for a symmetric thin airfoil at small angle of attack is given by  $c_l = 2\pi\alpha$ . Find the location of the control point (i.e. find the value of  $\eta$ ) such that the lift coefficient estimated from the simple point vortex model is identical to the thin airfoil results.